

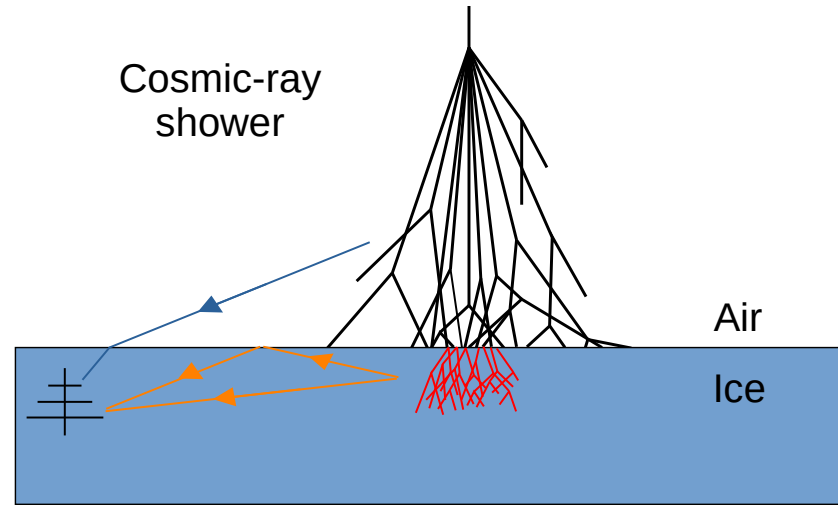
Propagating Air Showers Radio Signals to In-ice Antennas

Uzair Latif* (VUB), Simon de Kockere* (VUB), Tim Huege (KIT,
VUB), Krijn de Vries (VUB), Stijn Buitink (VUB), Dieder Van den
Broeck (VUB), Nick van Eindhoven (VUB)




Introduction

- We finally have a full cosmic ray shower simulation simulating radio emissions for in-ice antennas.
 - A combination of C7 and Geant4
- Currently analysing the initial results.
- The in-air (me) and the in-ice (Simon) emission codes are stable and are currently working with raytracing included.



Current Status

- In-air radio emission with ray tracing 

- In-ice radio emission with ray tracing 
 - Direct (1st) and Reflected/Refracted (2nd)

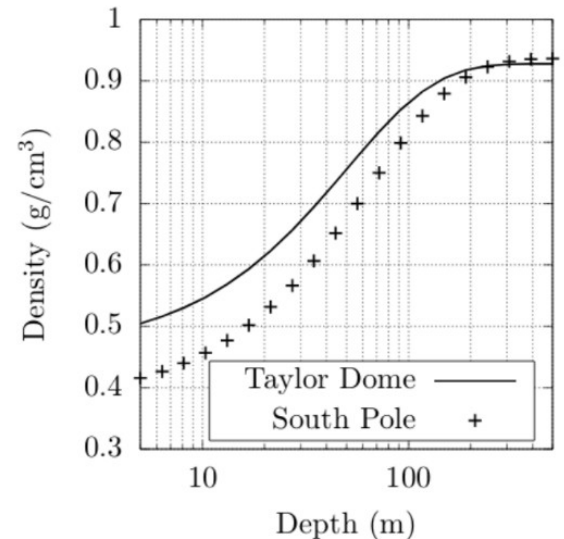
- Fresnel coefficients 

- Focusing/defocusing factor (in-ice) 

- Transition radiation (“for free”) 

Current Configuration

- Simulation of in-air particle development using CORSIKA 7.7500 with modified CoREAS
 - Proton, Energy 1×10^{17} eV
 - QGSJETII-04 (HE), UrQMD (LE)
 - Thinning
 - Particle read-out at altitude of 2.835 km asl
- Simulation of in-ice propagation using Geant4 10.5
 - Propagation of all CORSIKA output particles within 1 m of core.
 - Using realistic ice density gradient
 - End-point formalism for radio emission

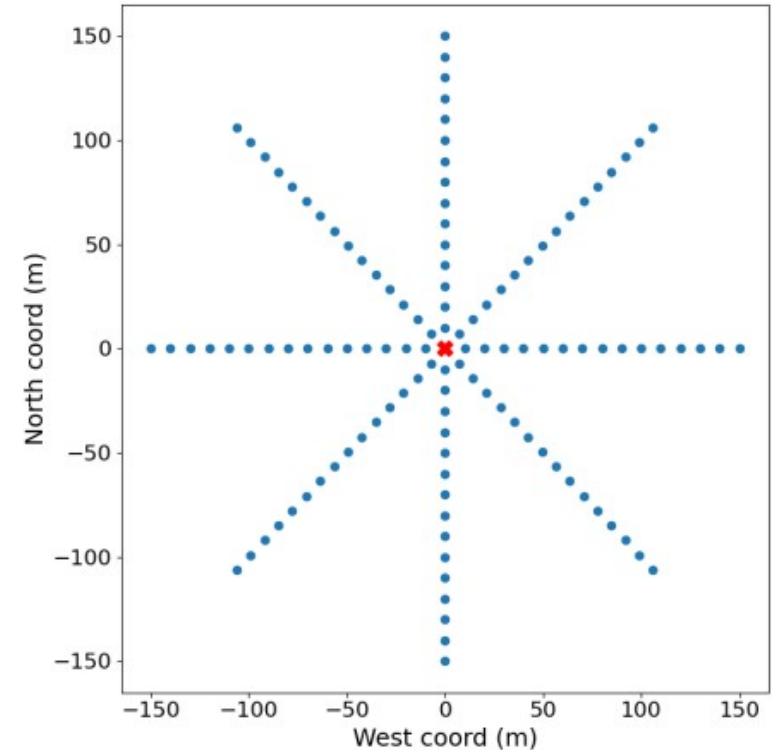


Other details

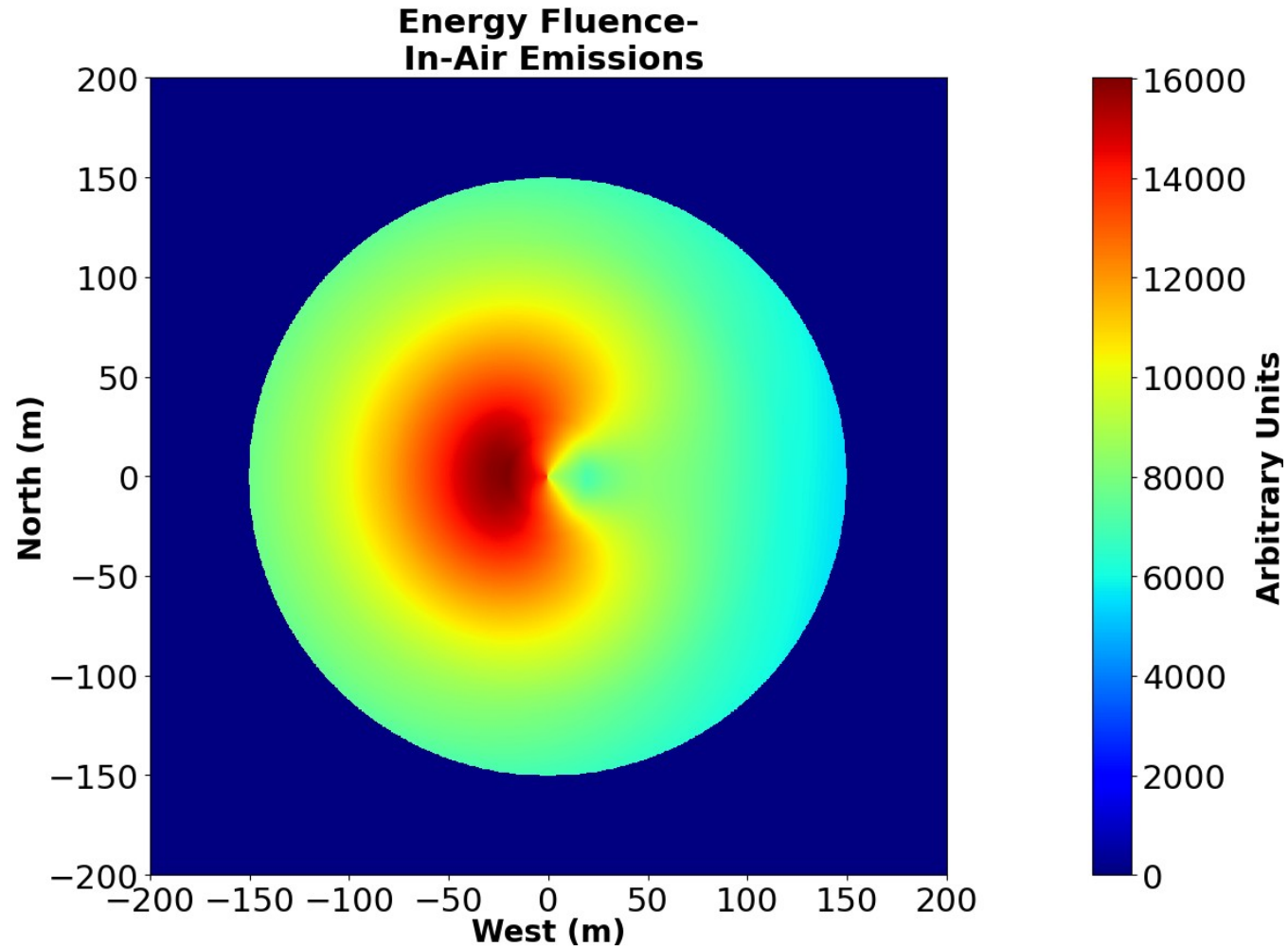
- Raytracing implemented using interpolation
 - Helps account for non-linear refractive index profiles
- Focusing factor formula taken from NuRadioMC
 - Limited to a maximum of 2

Shower Geometry

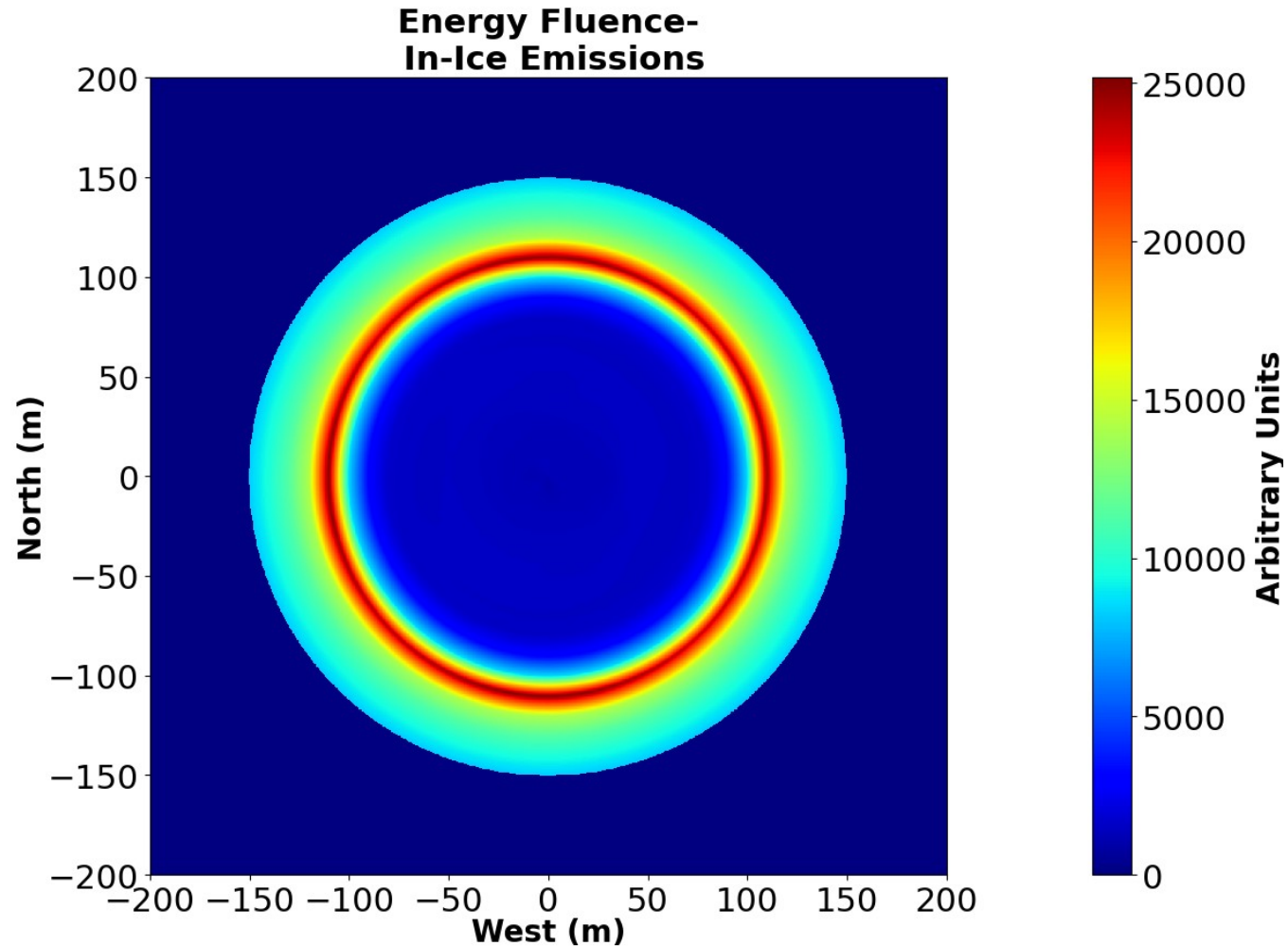
- Vertical Proton Shower at 10^{17} eV
- Ice layer at around 2.85 km a.s.l
- Antenna Star at -150 m depth.
- Shower core hitting at the center of the star.



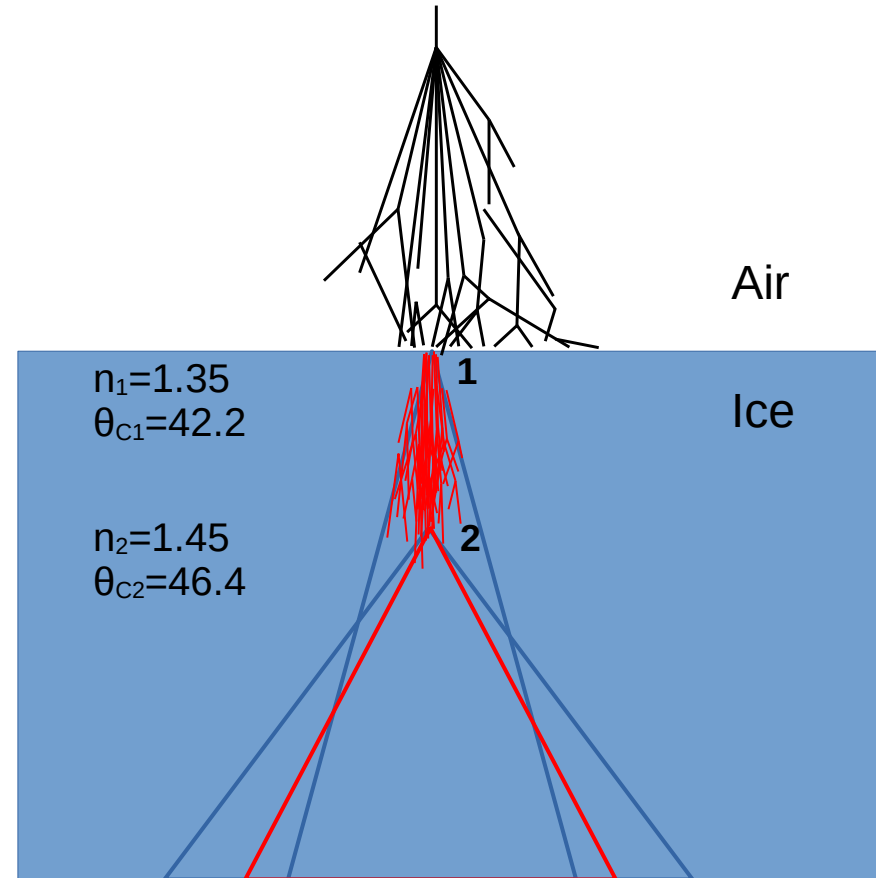
- In-air emission generates both Askayran and geomagnetic emission, interference explains the asymmetry
- Very similar to radio footprint on the surface



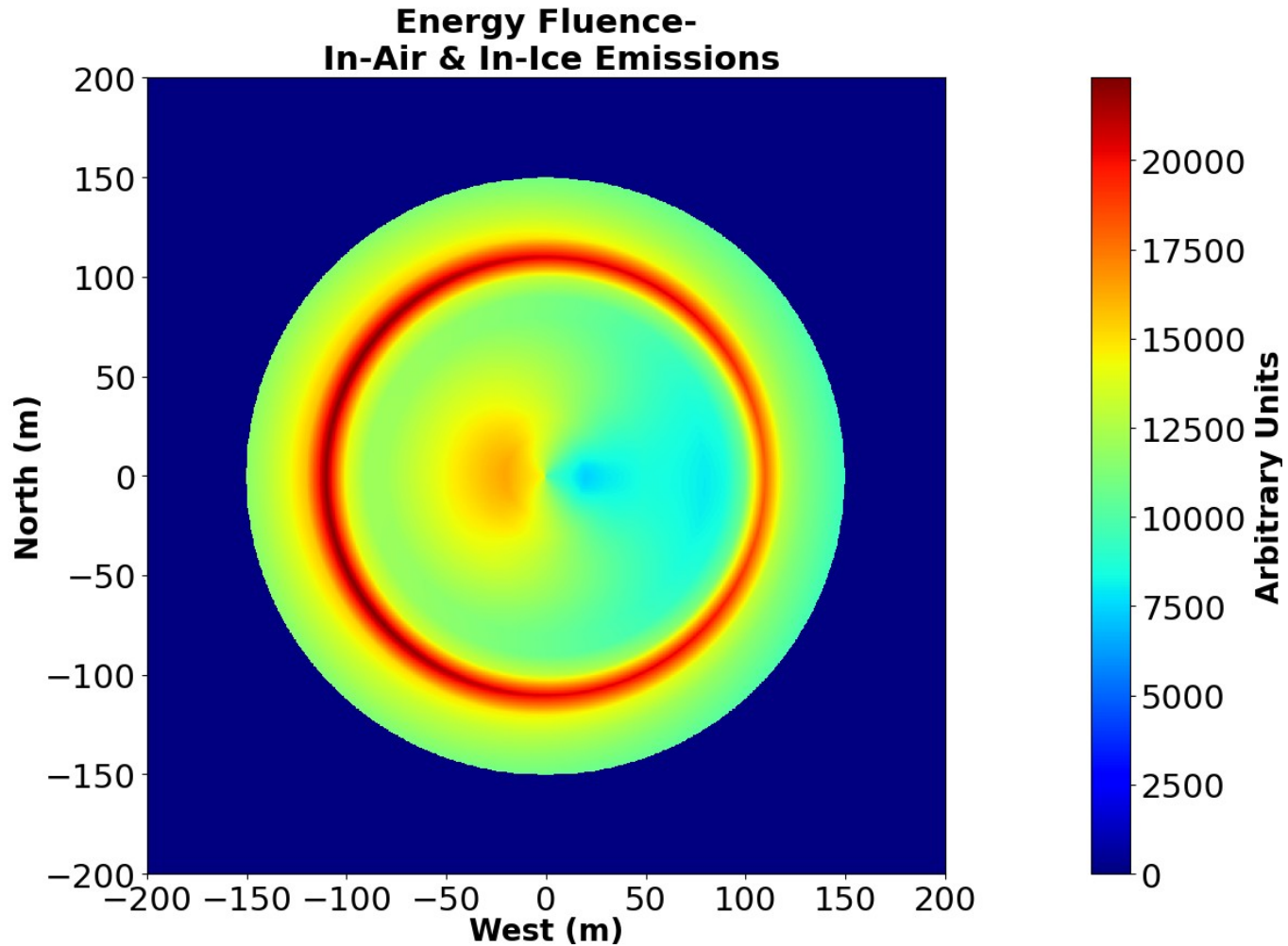
- In-ice emission only generates Askaryan emission, giving a very symmetric pattern
- Cherenkov ring clearly visible, as cascade in the ice is very compact $O(5-10\text{ m})$, concentrating emission in small opening angle.
- Spread in Cherenkov ring due to shower evolution in ice.



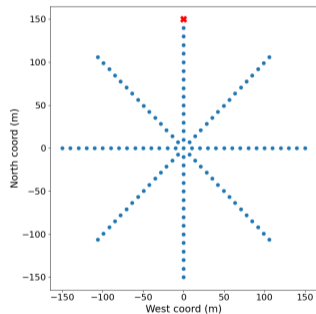
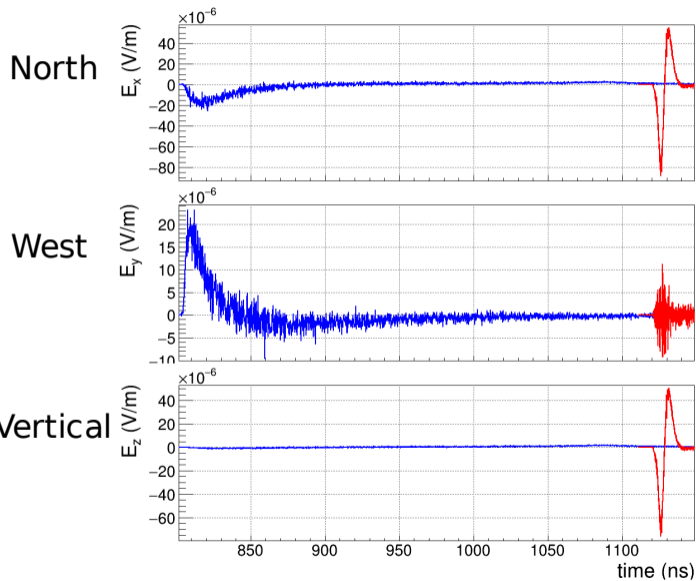
Spread of In-Ice Cherenkov Cone



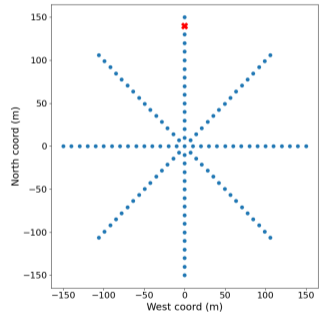
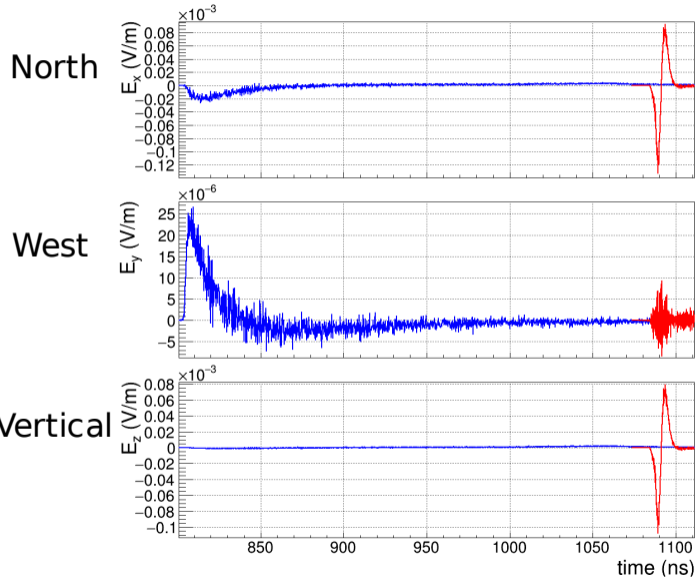
- In-air emission illuminates the center, while in-ice emission is very concentrated around its Cherenkov ring
- Slight asymmetry in ring due to interference with geomagnetic in-air emission.



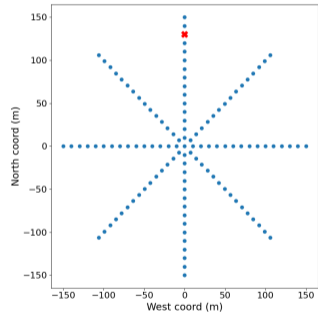
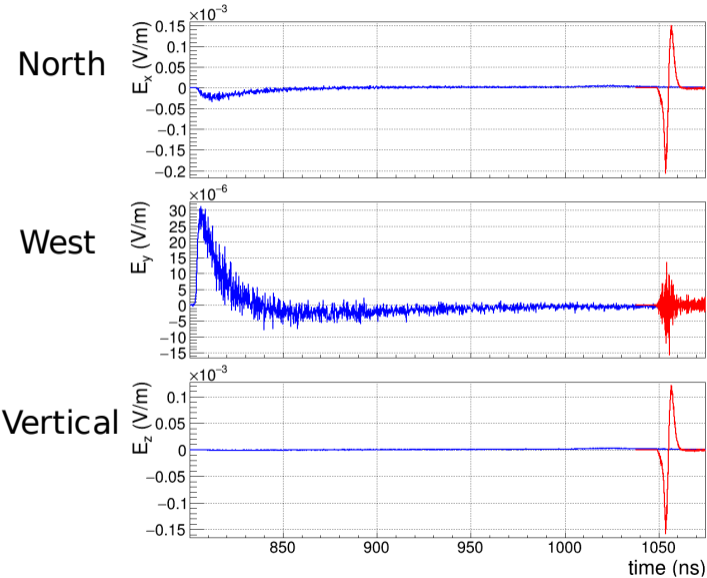
E for shower with $E_p = 10^{17}$ eV, $\theta = 0$, depth = -150 m



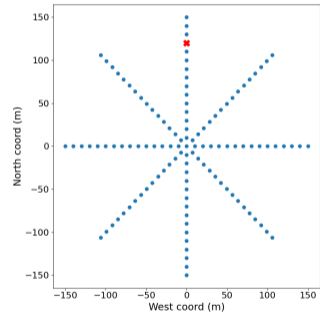
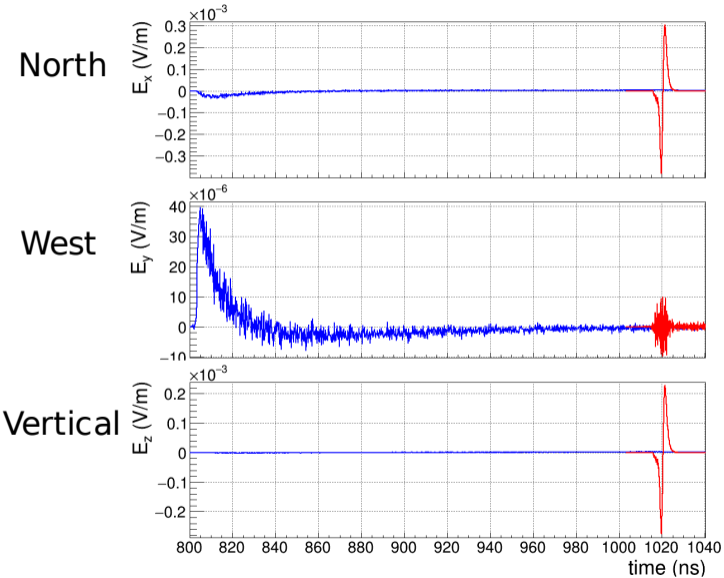
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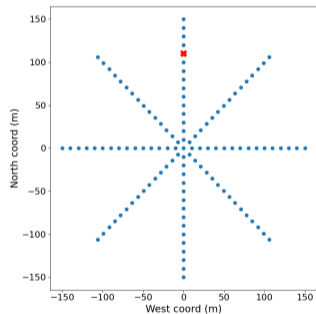
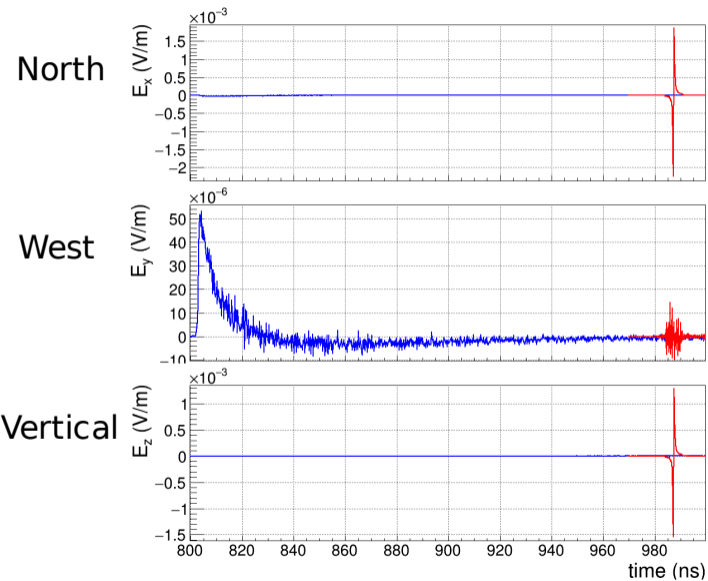
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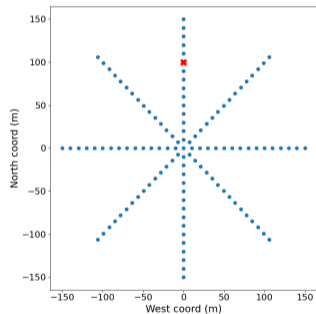
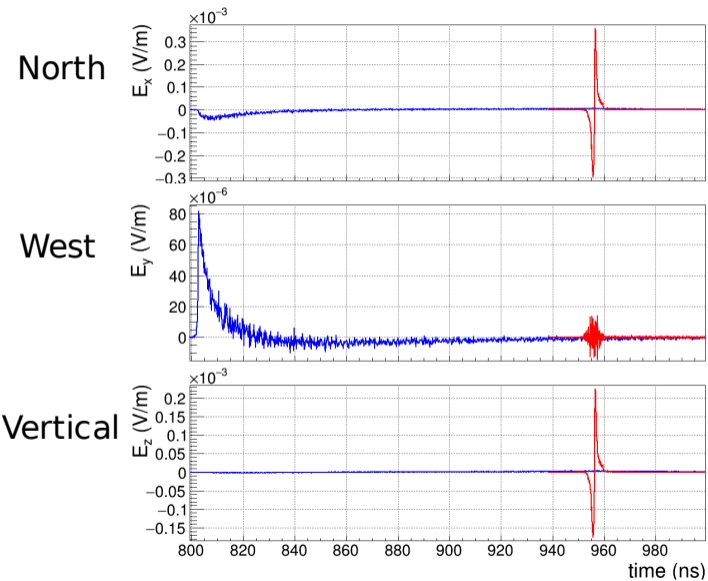
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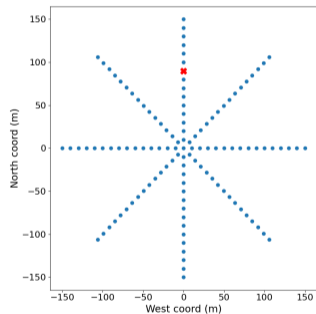
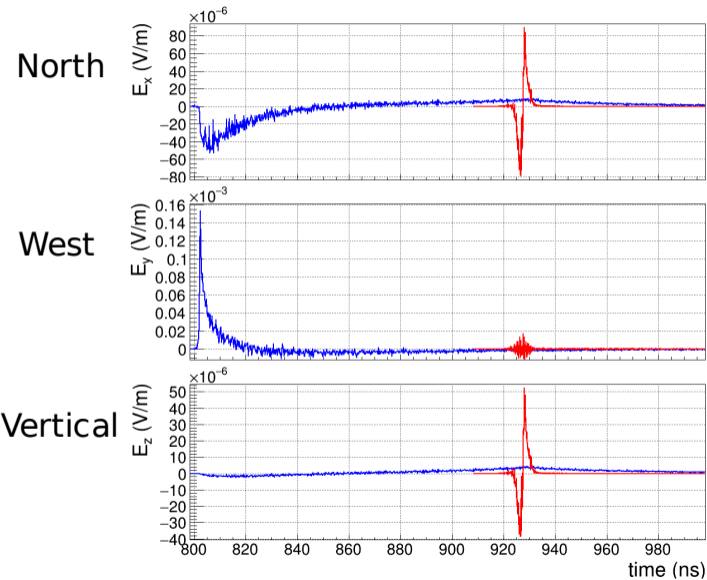
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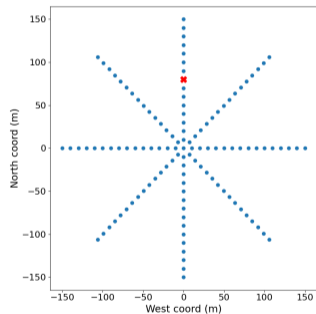
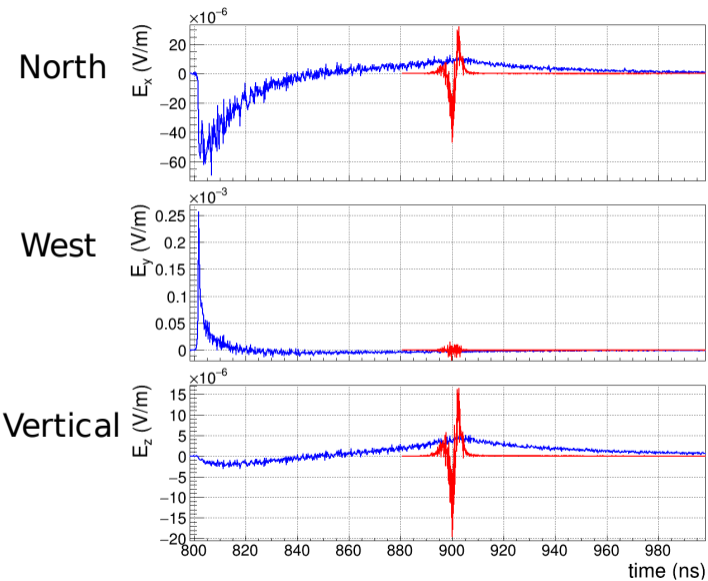
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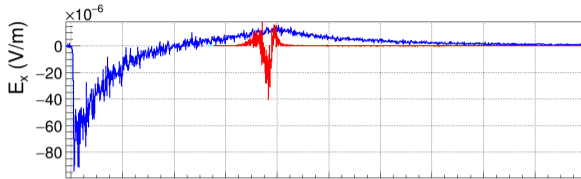


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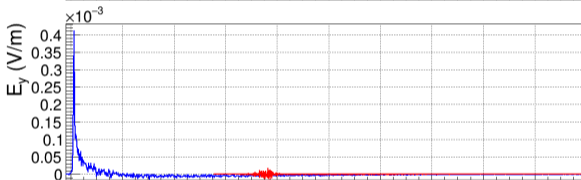


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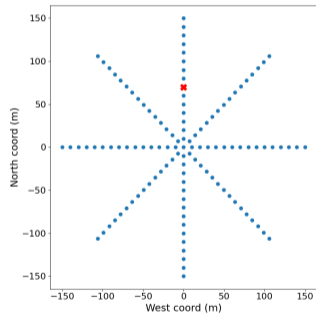
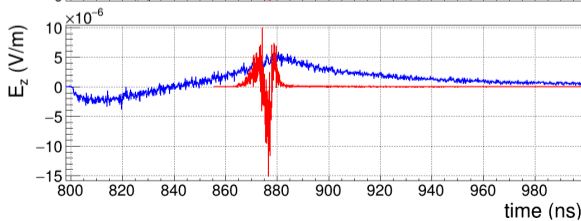
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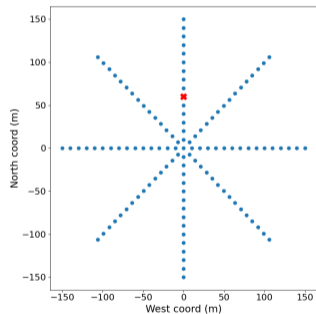
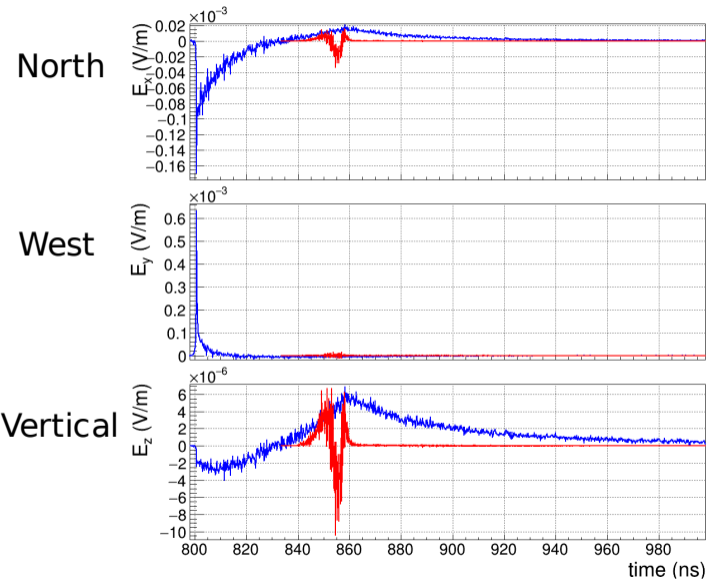
West



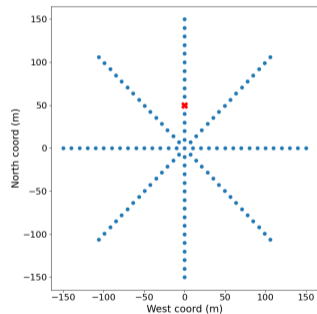
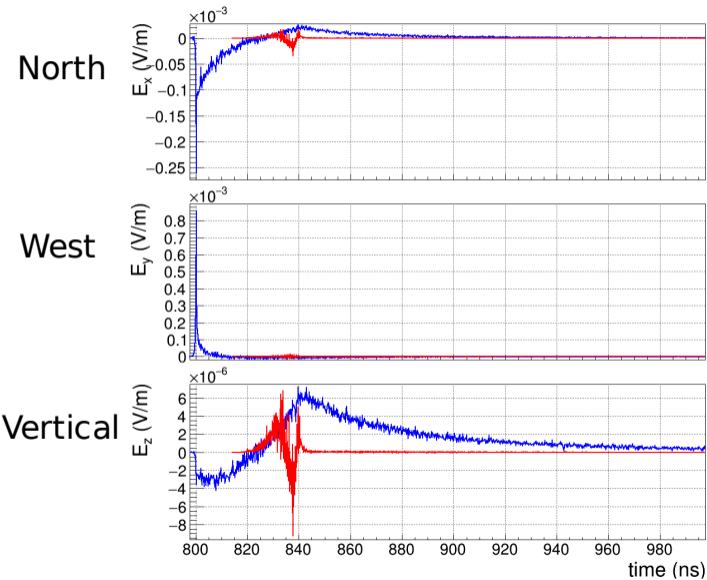
Vertical



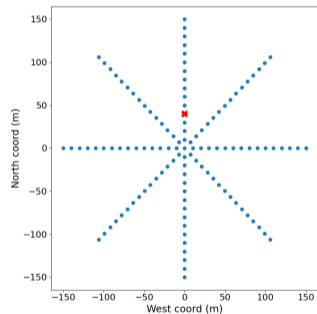
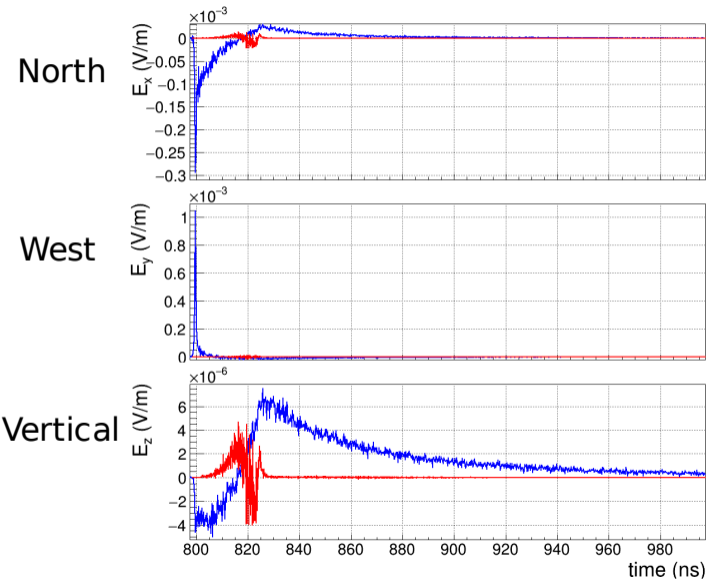
E for shower with $E_p = 10^{17}$ eV, $\theta = 0$, depth = -150 m



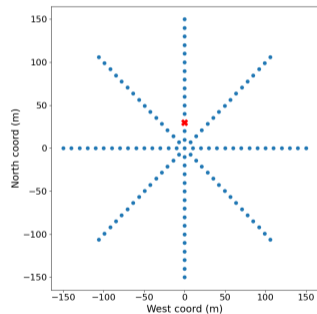
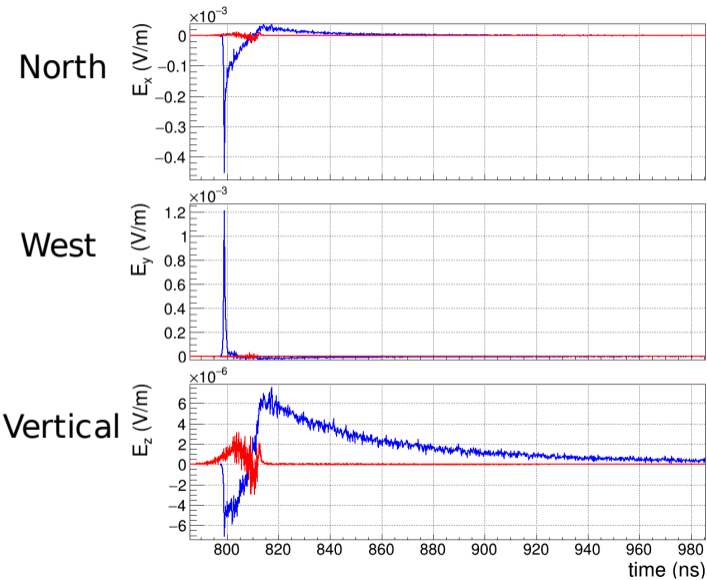
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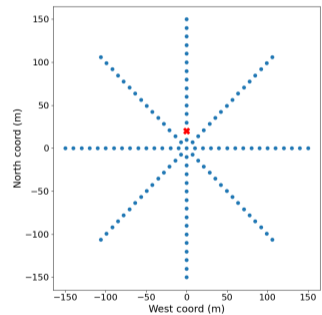
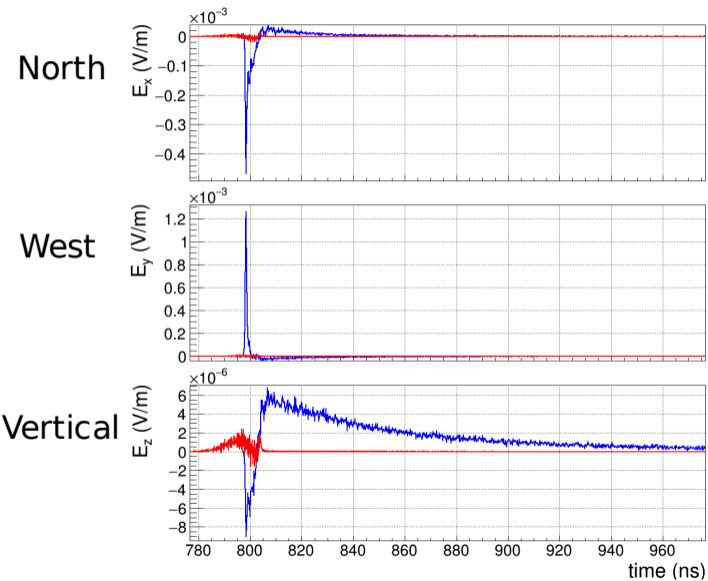
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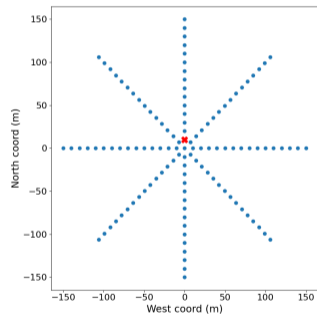
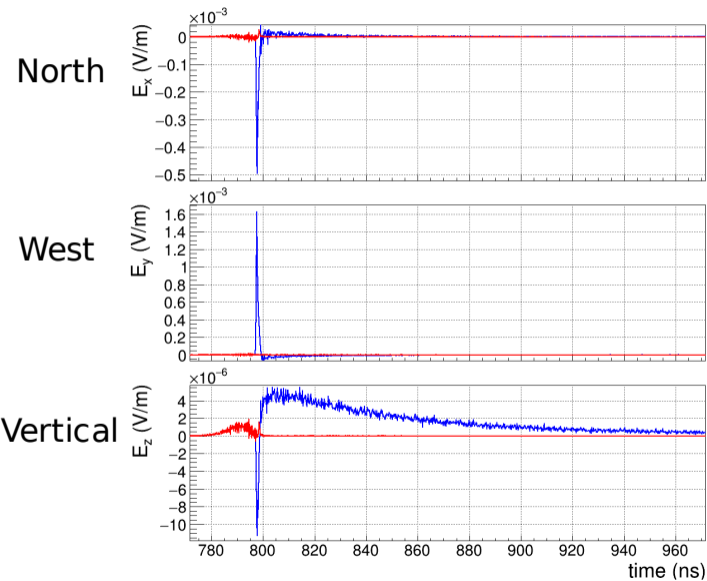
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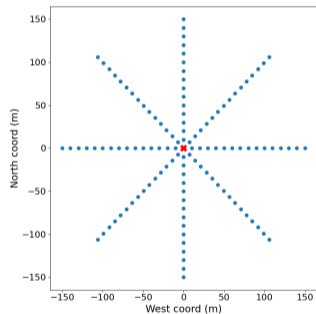
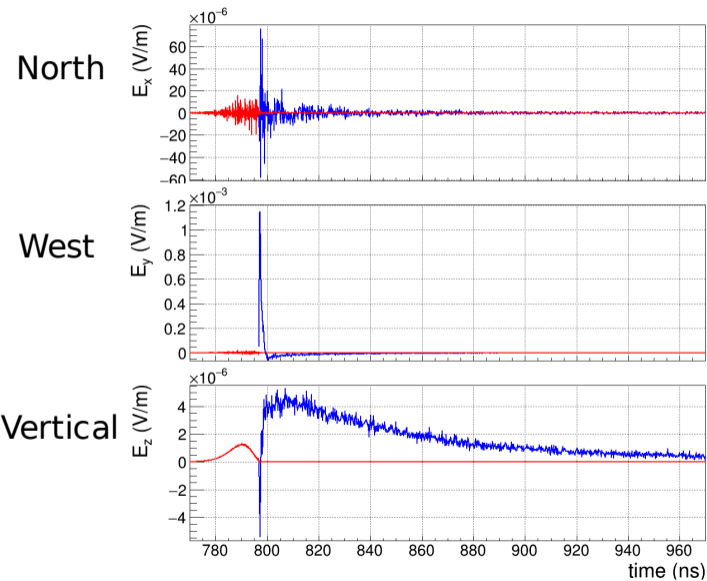
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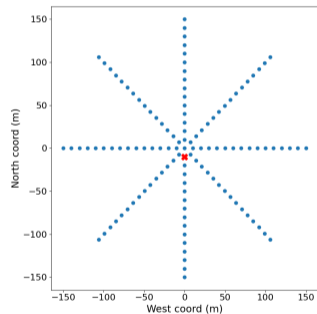
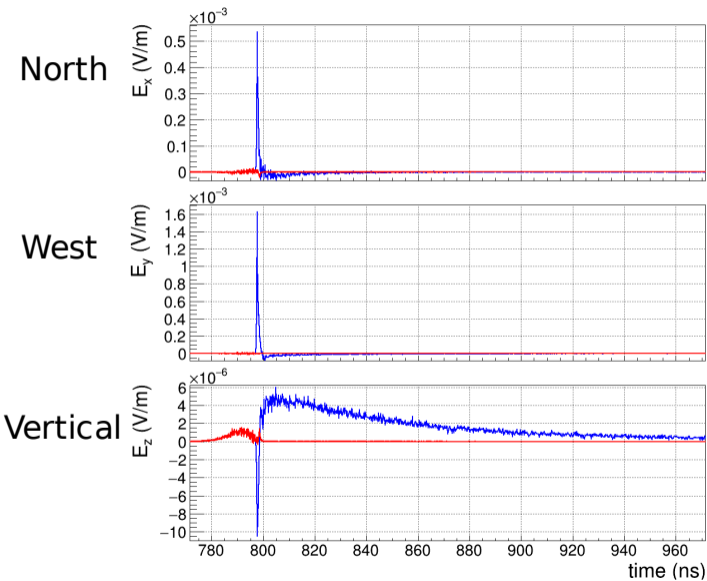
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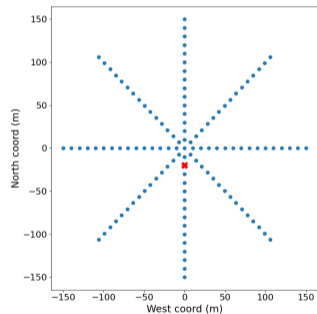
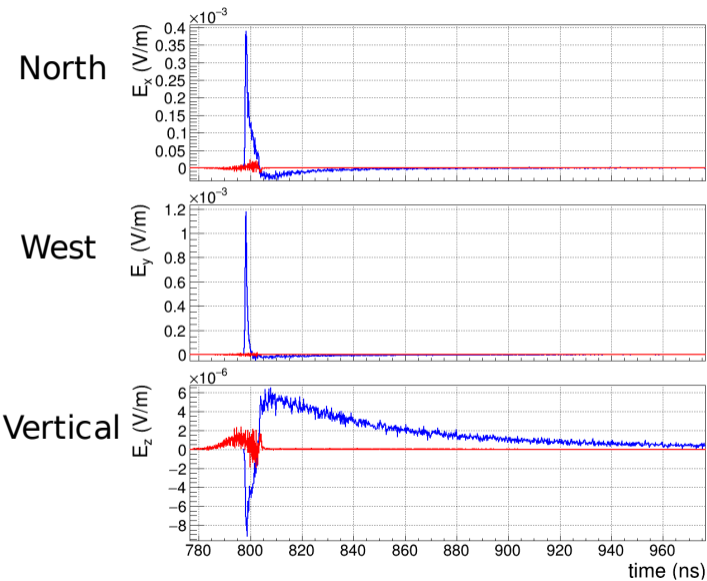
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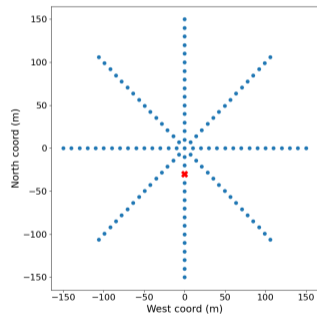
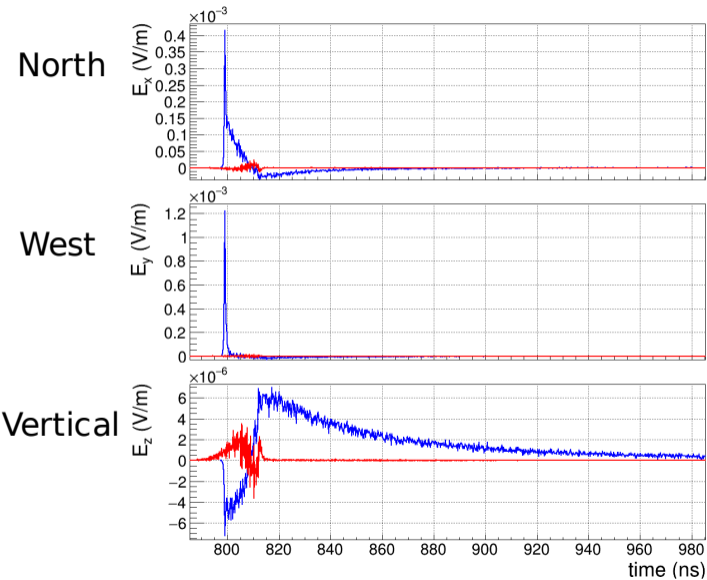
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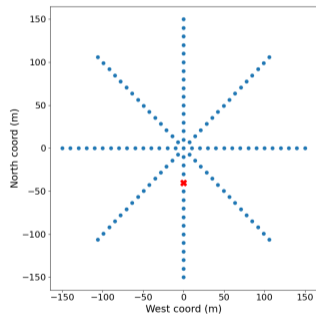
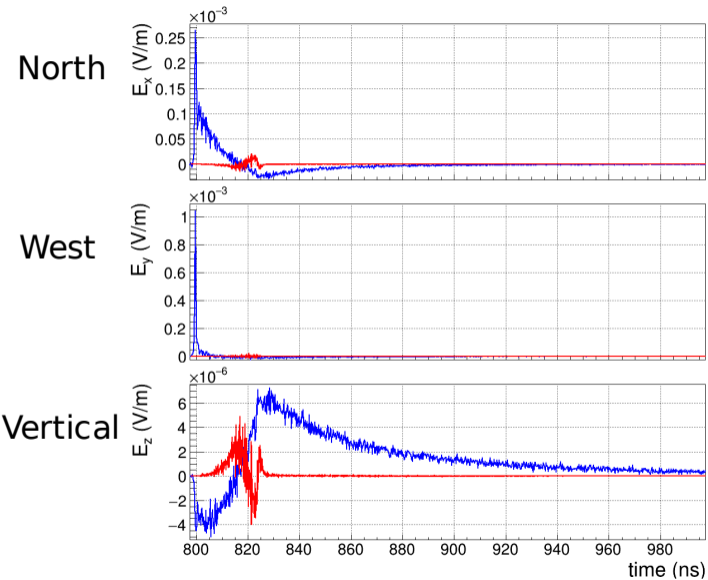
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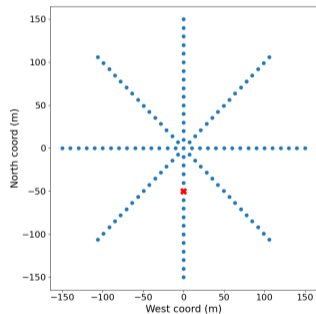
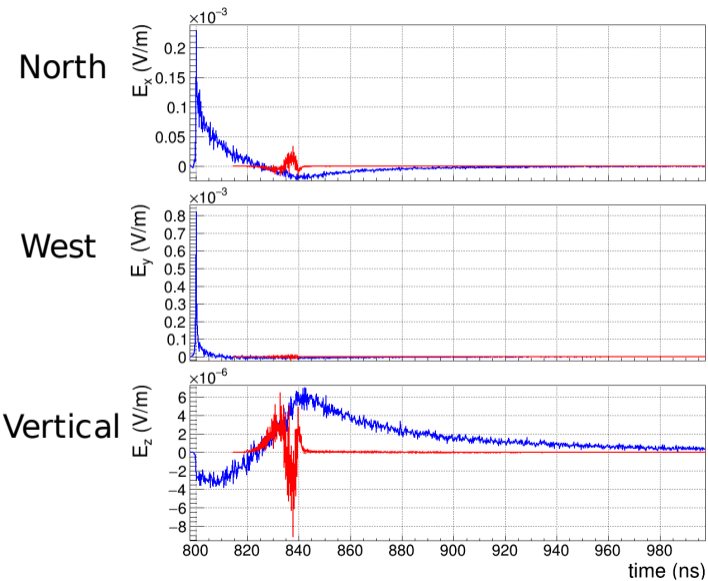
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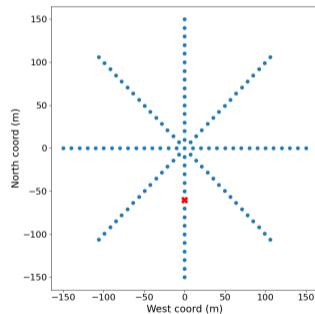
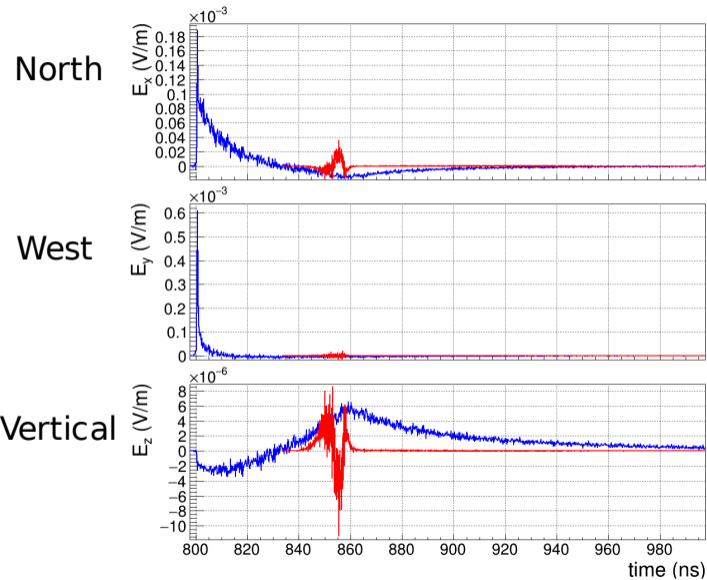
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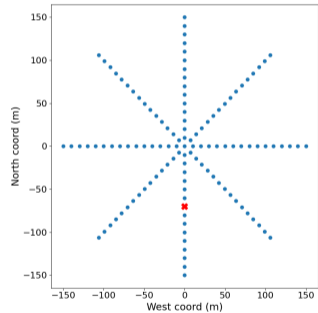
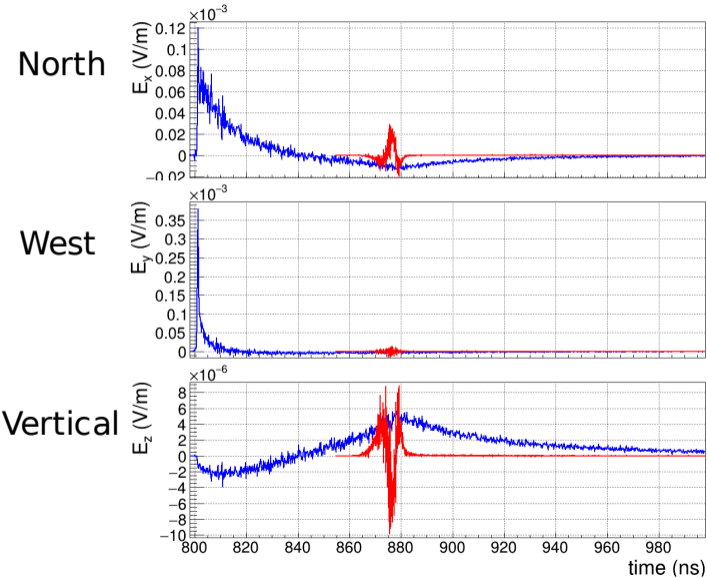
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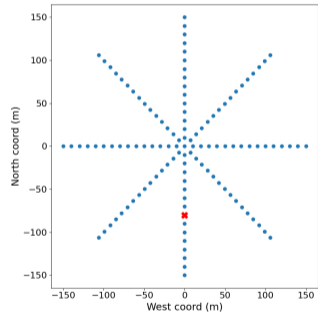
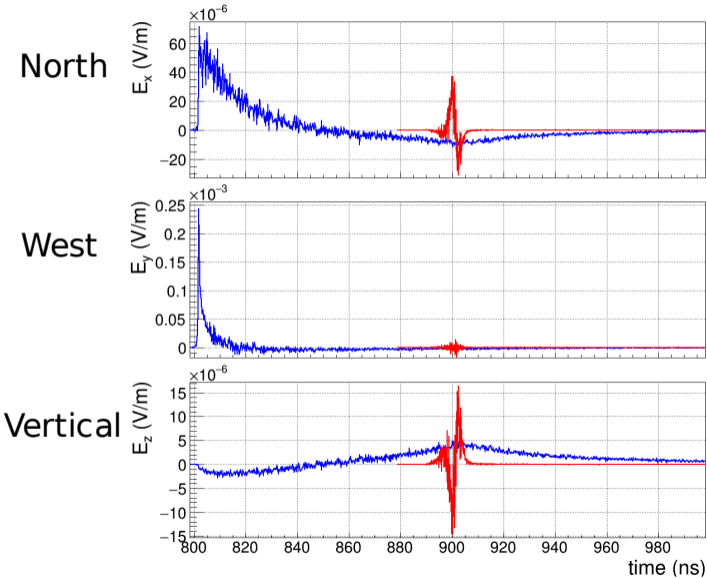
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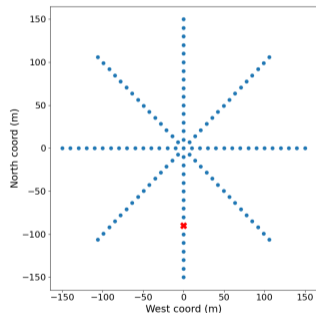
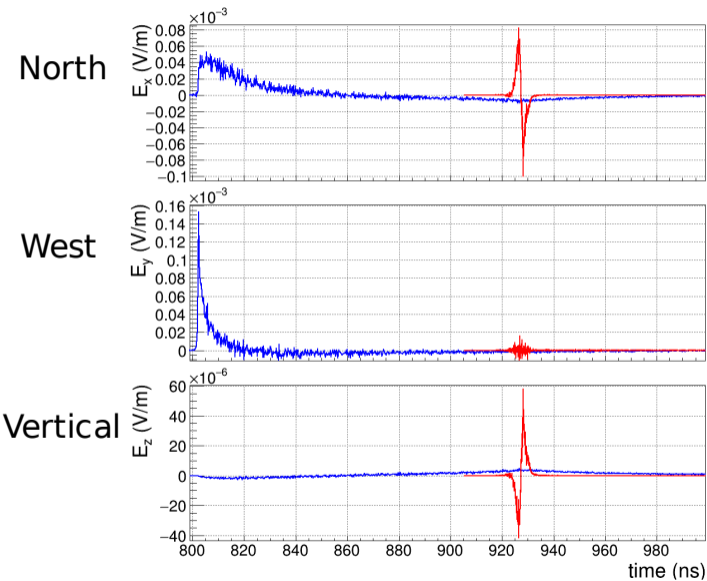
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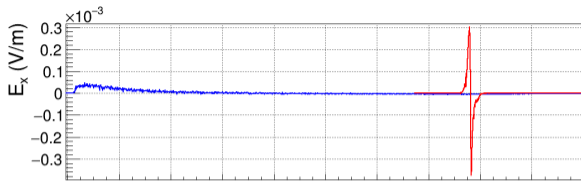


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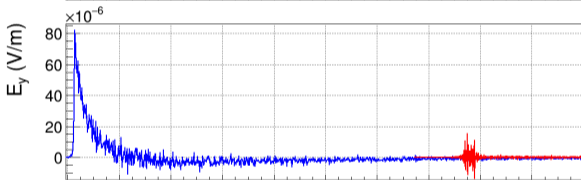


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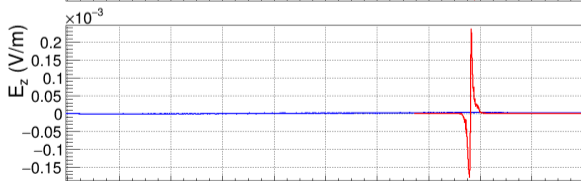
North



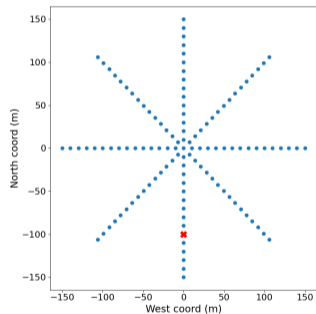
West



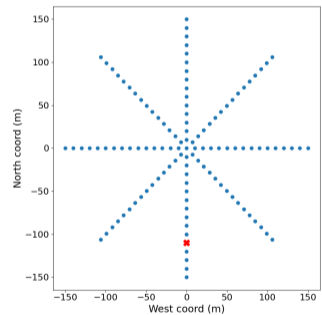
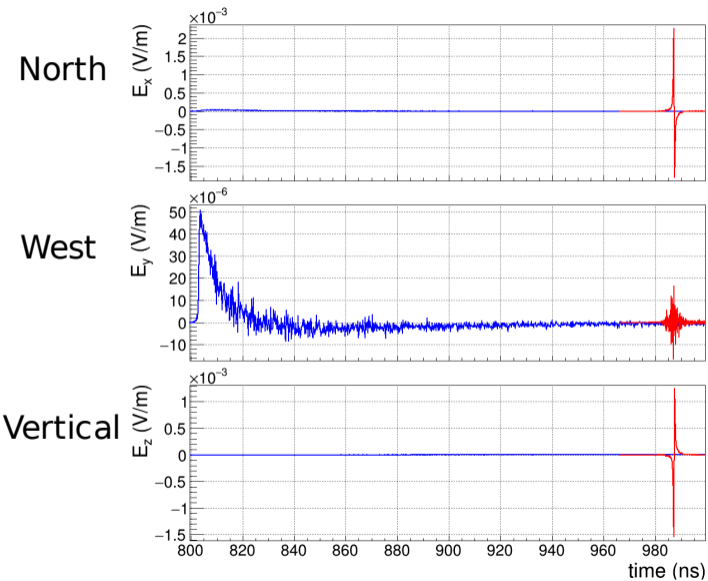
Vertical



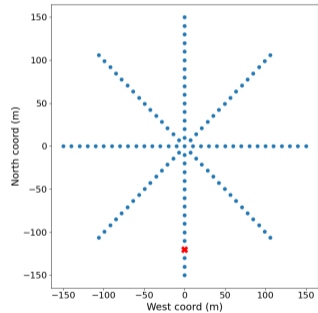
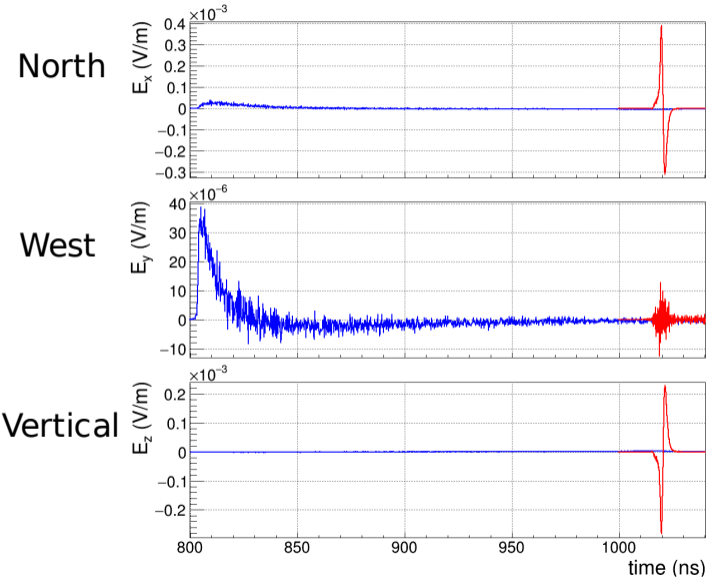
time (ns)



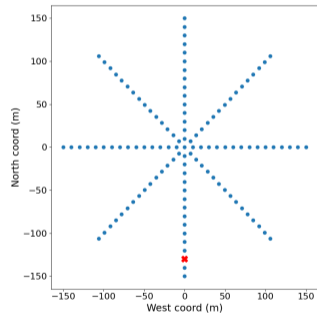
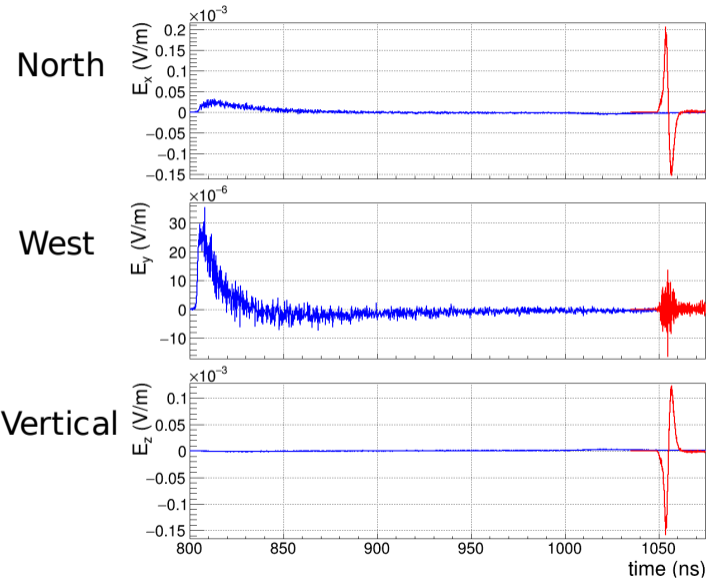
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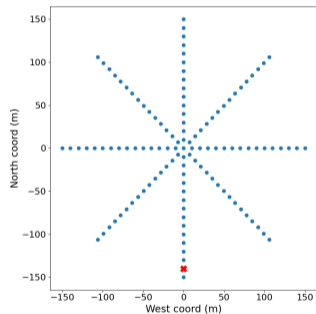
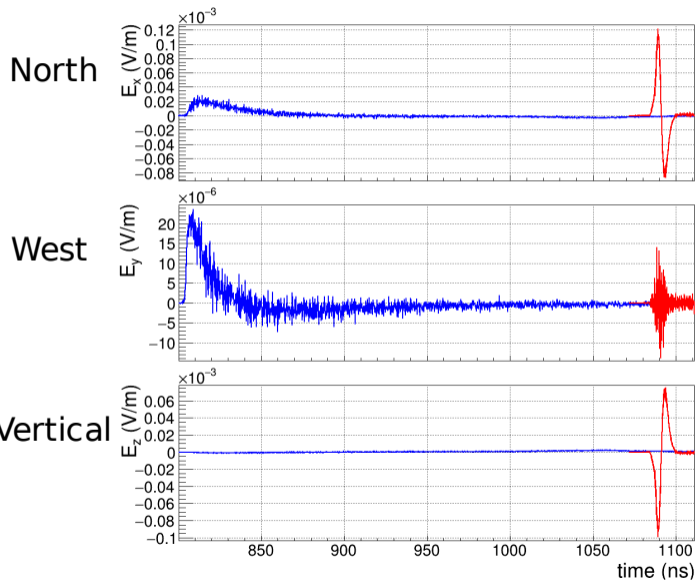
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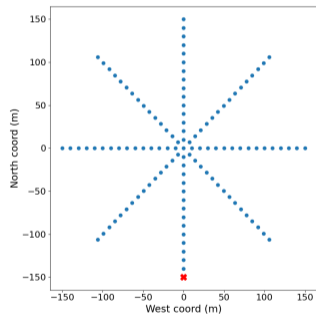
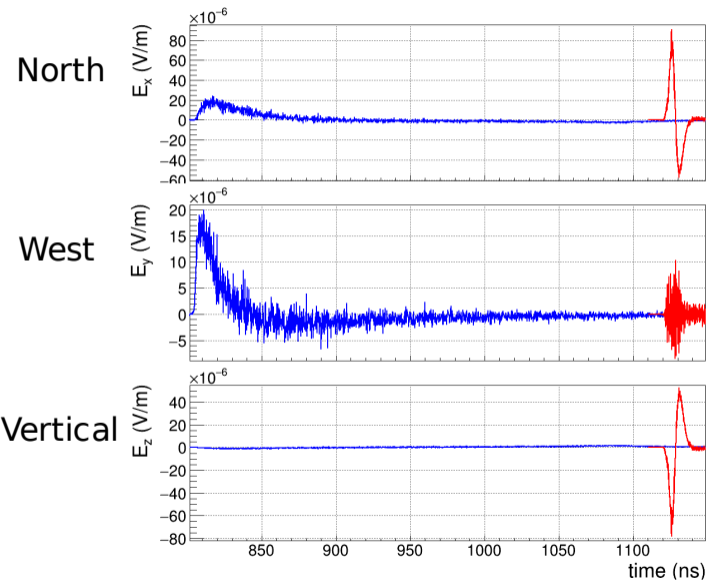
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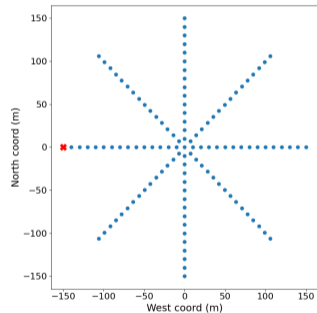
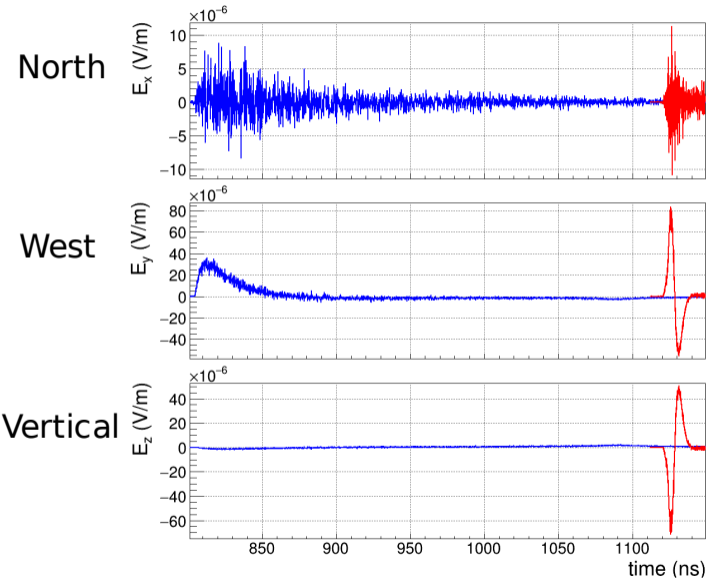
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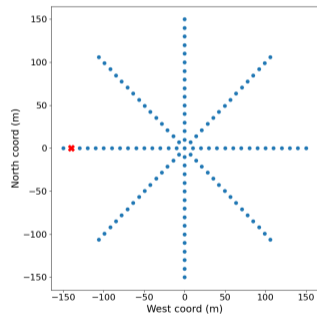
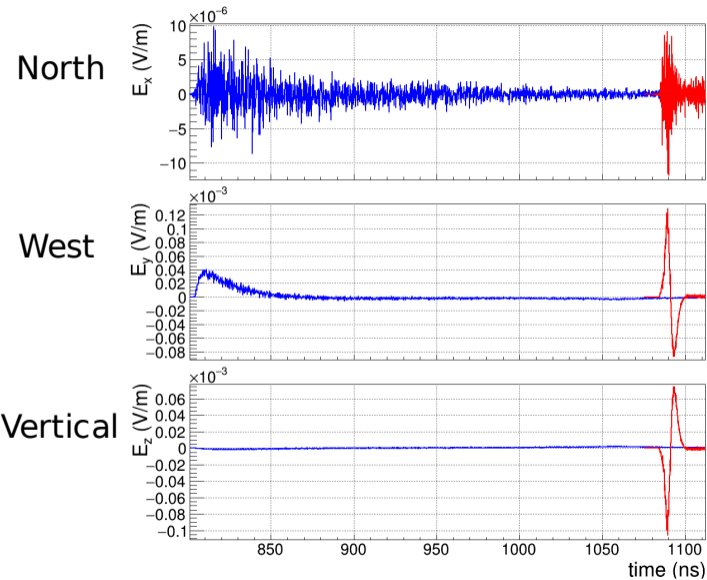
E for shower with $E_p = 10^{17}$ eV, $\theta = 0$, depth = -150 m



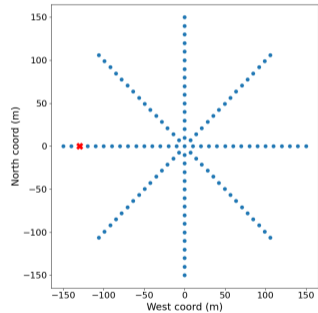
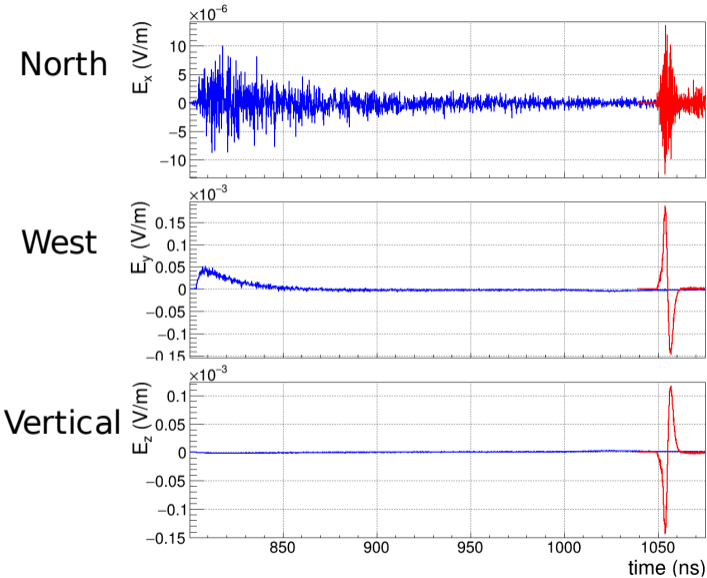
E for shower with $E_p = 10^{17}$ eV, $\theta = 0$, depth = -150 m



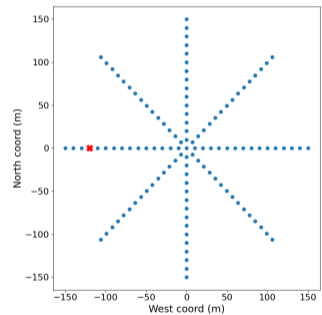
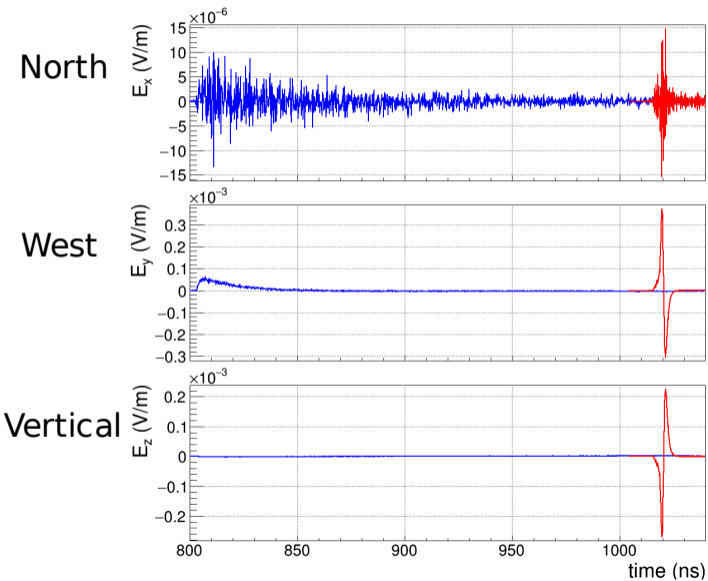
E for shower with $E_p = 10^{17}$ eV, $\theta = 0$, depth = -150 m



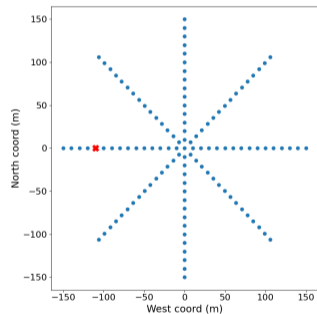
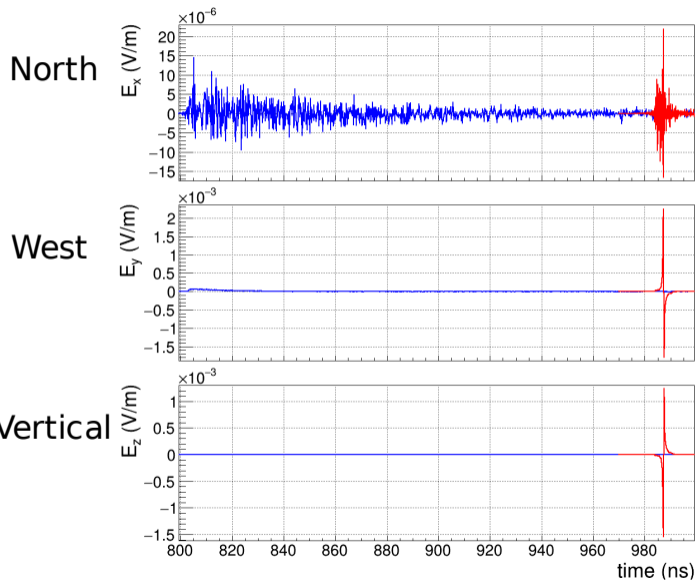
E for shower with $E_p = 10^{17}$ eV, $\theta = 0$, depth = -150 m



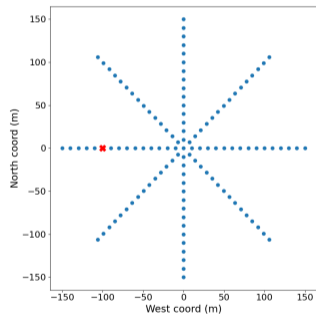
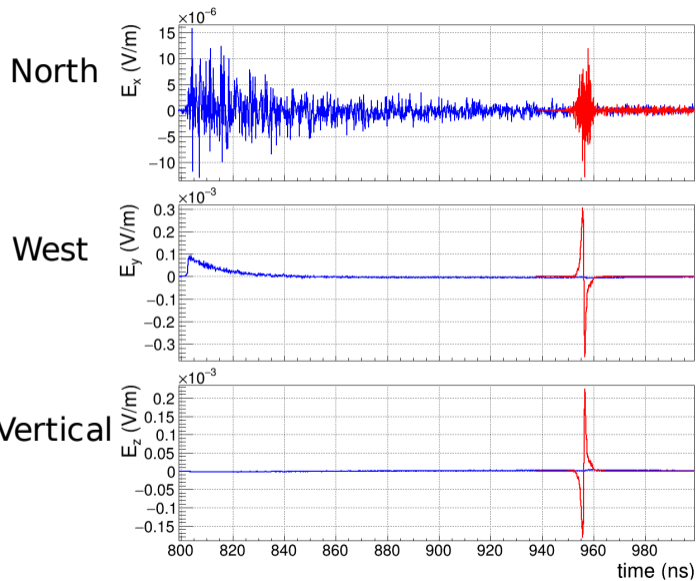
E for shower with $E_p = 10^{17}$ eV, $\theta = 0$, depth = -150 m



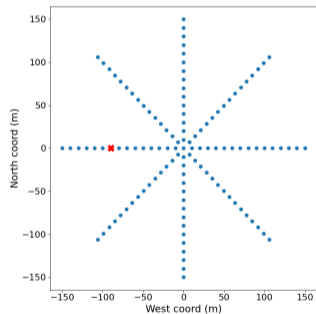
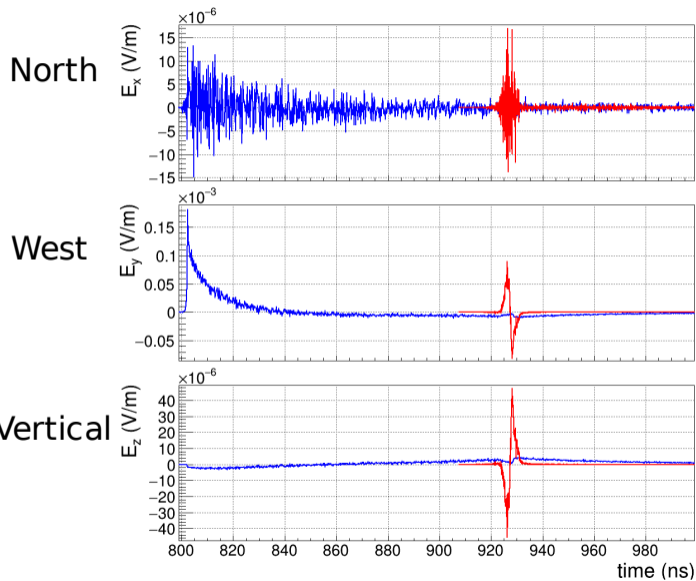
E for shower with $E_p = 10^{17}$ eV, $\theta = 0$, depth = -150 m



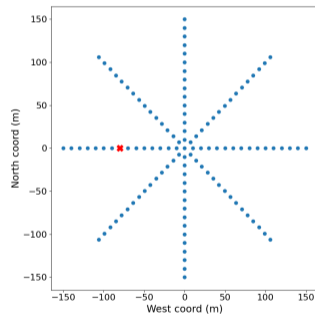
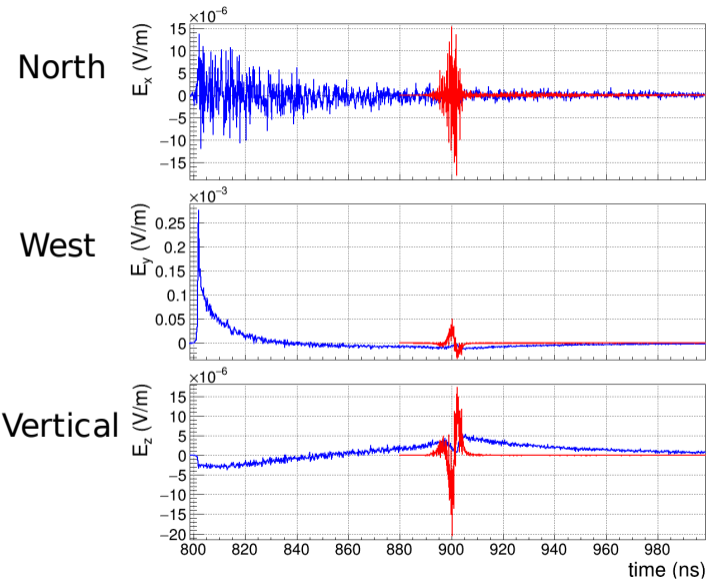
E for shower with $E_p = 10^{17}$ eV, $\theta = 0$, depth = -150 m



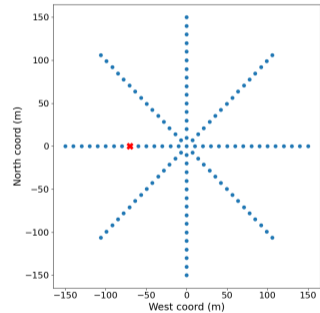
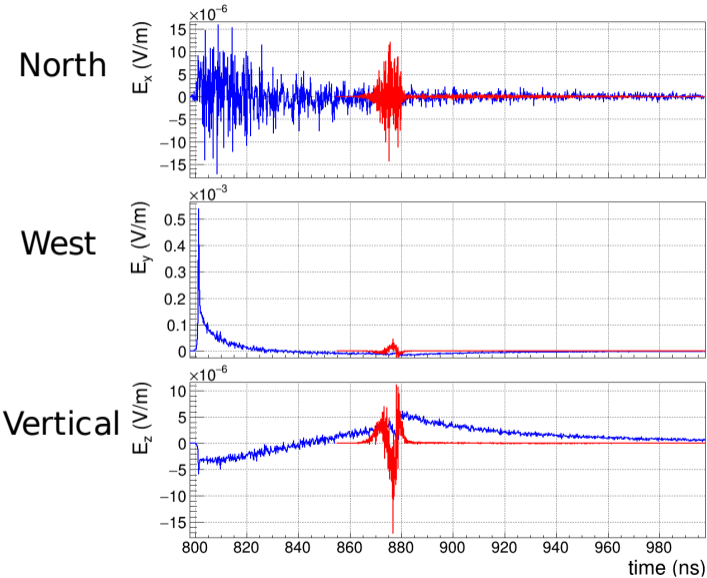
E for shower with $E_p = 10^{17}$ eV, $\theta = 0$, depth = -150 m



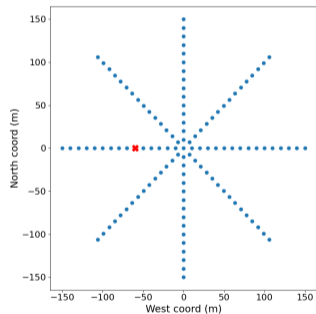
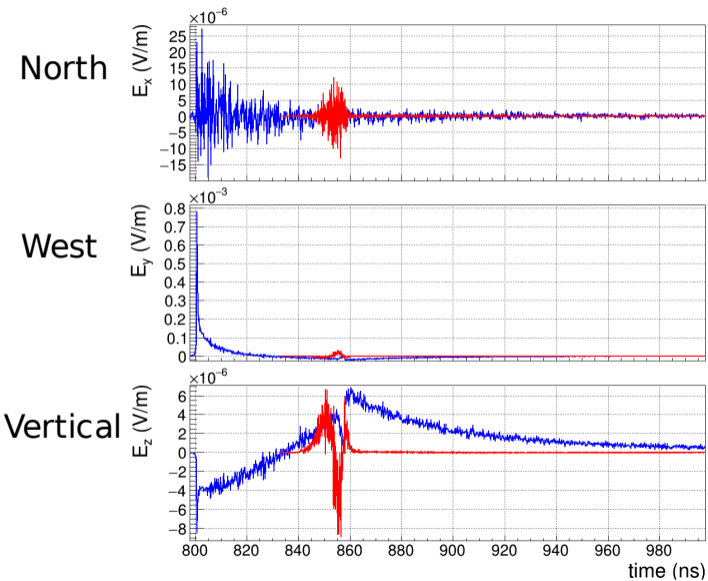
E for shower with $E_p = 10^{17}$ eV, $\theta = 0$, depth = -150 m



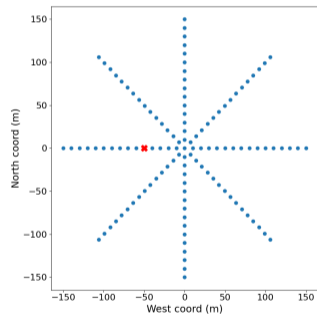
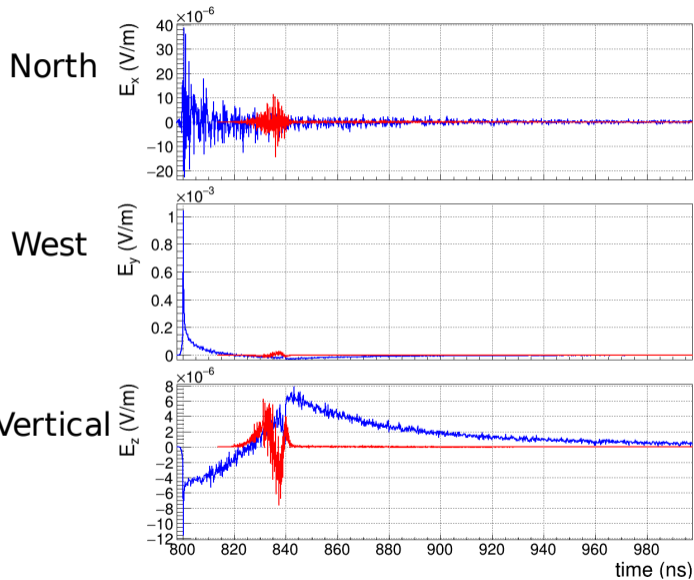
E for shower with $E_p = 10^{17}$ eV, $\theta = 0$, depth = -150 m



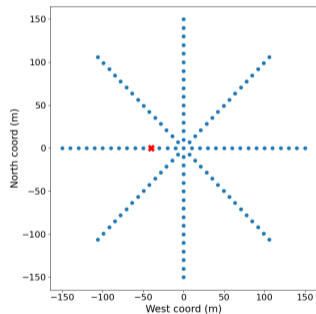
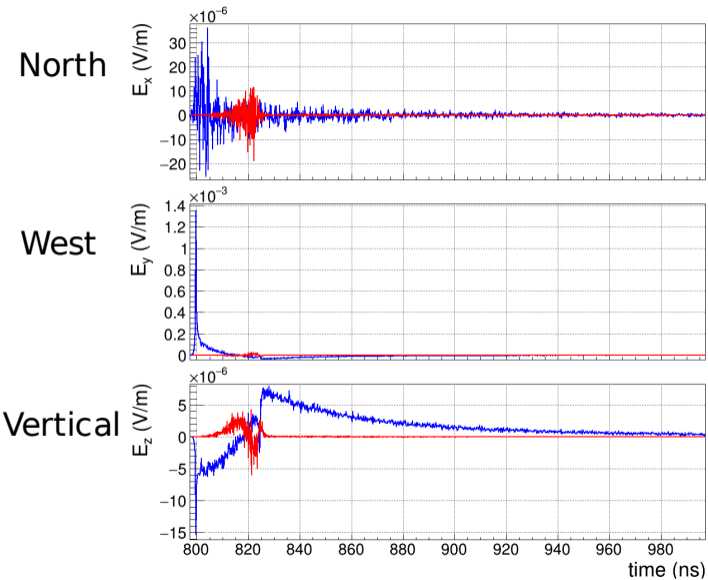
E for shower with $E_p = 10^{17}$ eV, $\theta = 0$, depth = -150 m



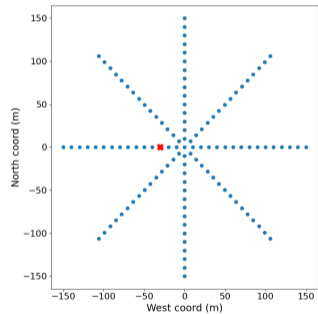
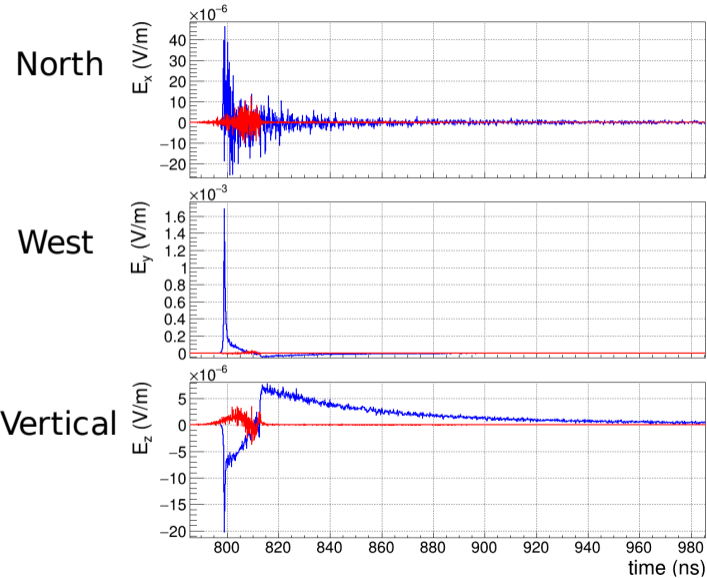
E for shower with $E_p = 10^{17}$ eV, $\theta = 0$, depth = -150 m



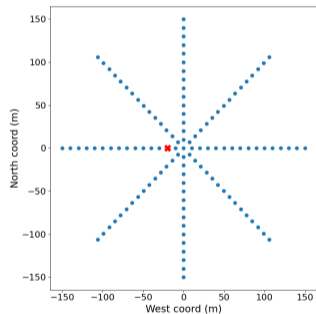
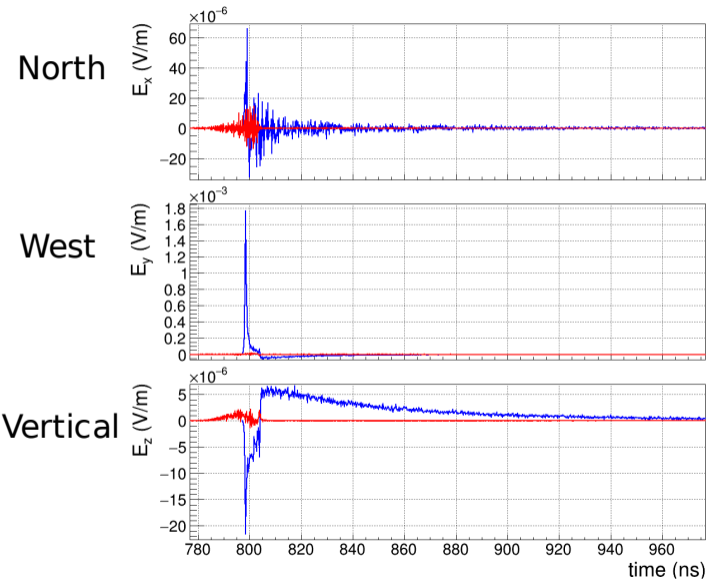
E for shower with $E_p = 10^{17}$ eV, $\theta = 0$, depth = -150 m



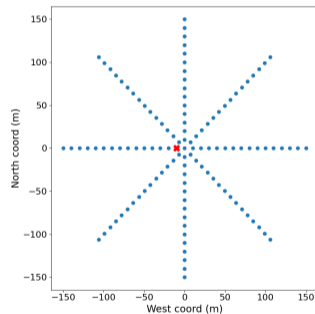
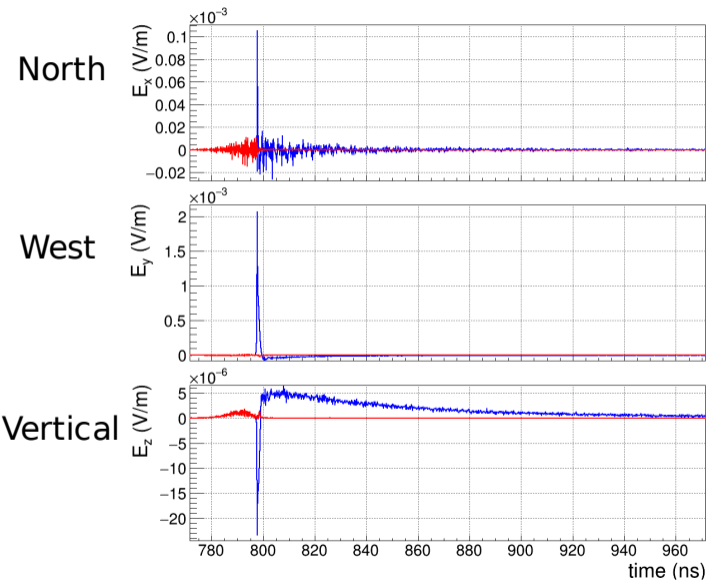
E for shower with $E_p = 10^{17}$ eV, $\theta = 0$, depth = -150 m



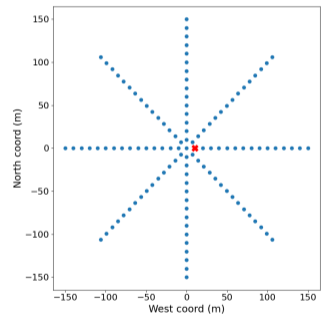
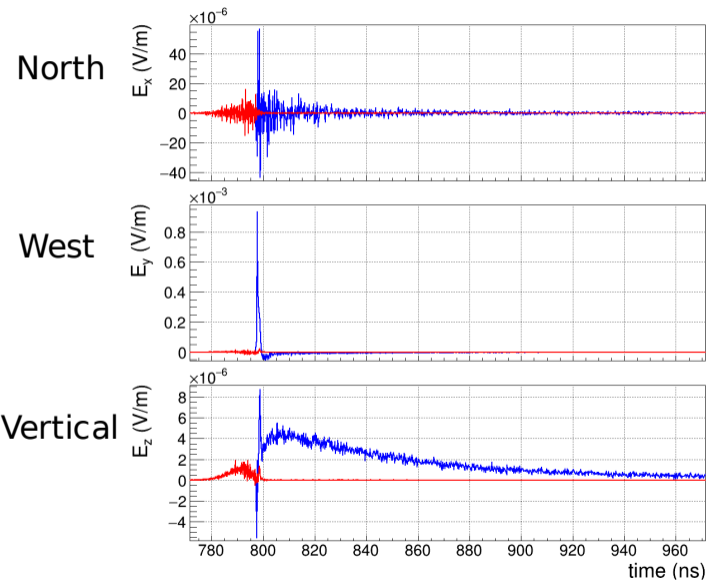
E for shower with $E_p = 10^{17}$ eV, $\theta = 0$, depth = -150 m



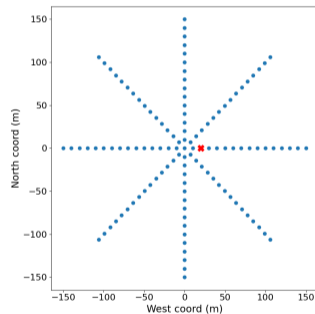
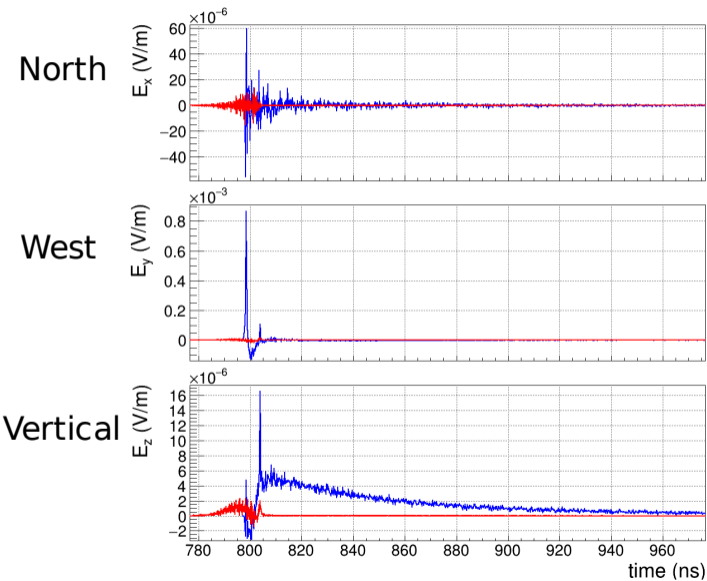
E for shower with $E_p = 10^{17}$ eV, $\theta = 0$, depth = -150 m



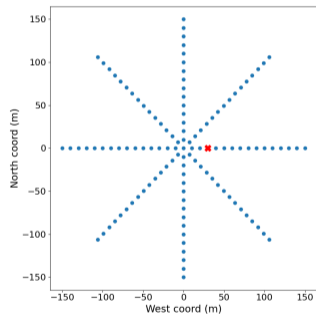
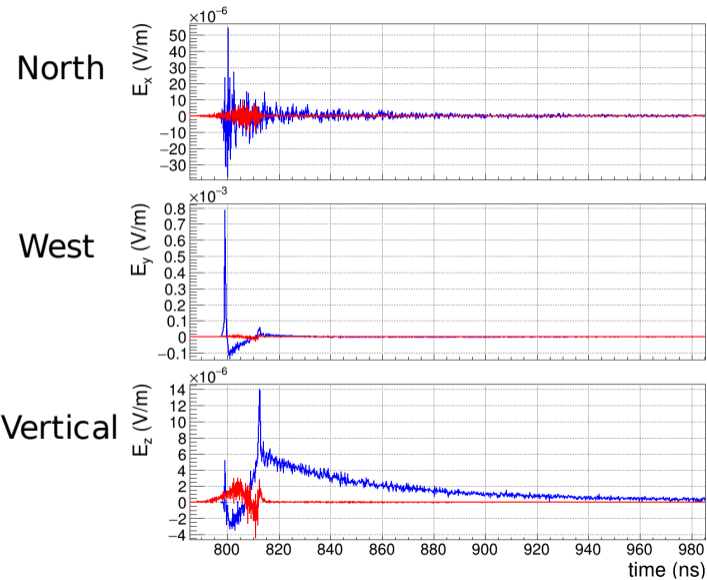
E for shower with $E_p = 10^{17}$ eV, $\theta = 0$, depth = -150 m



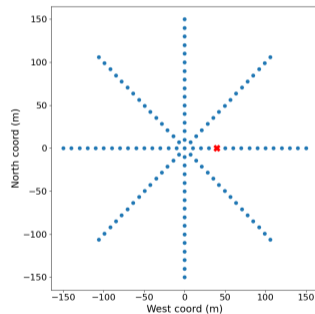
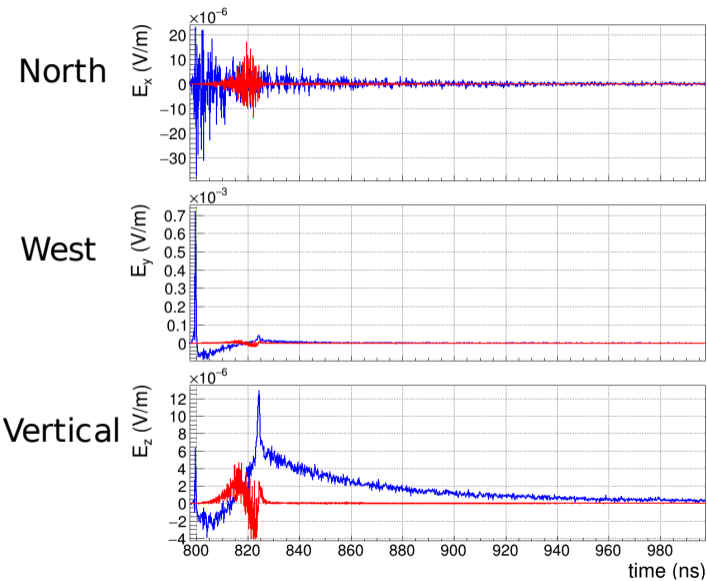
E for shower with $E_p = 10^{17}$ eV, $\theta = 0$, depth = -150 m



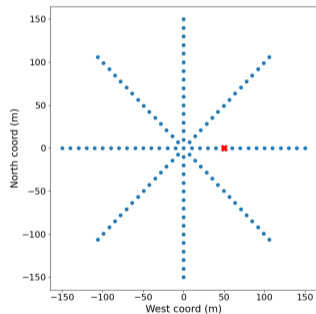
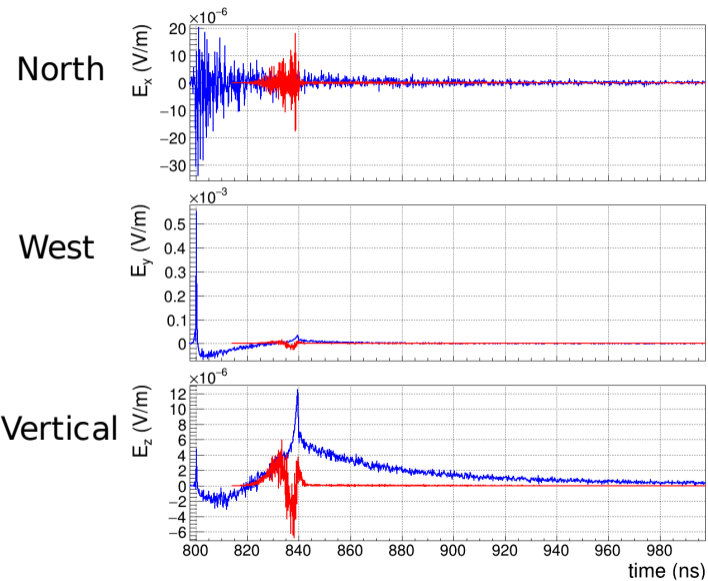
E for shower with $E_p = 10^{17}$ eV, $\theta = 0$, depth = -150 m



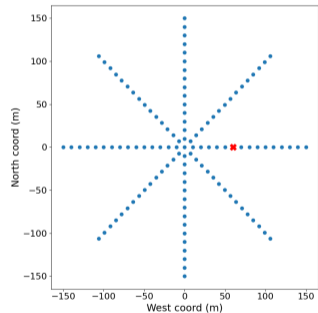
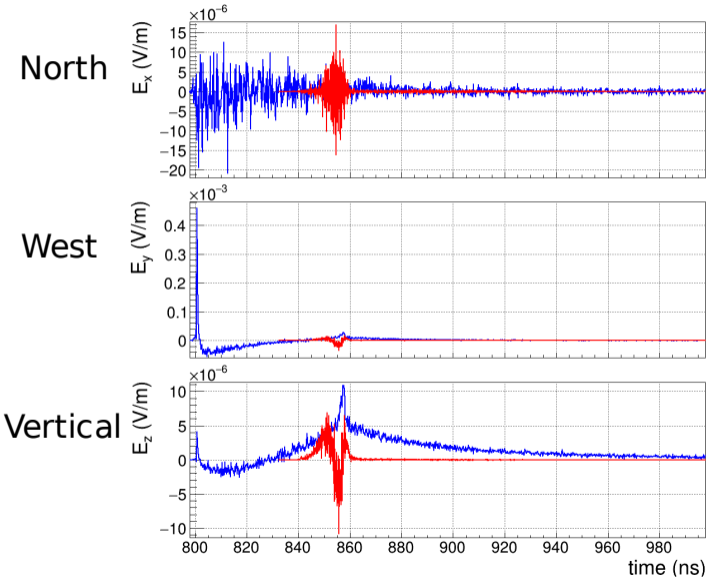
E for shower with $E_p = 10^{17}$ eV, $\theta = 0$, depth = -150 m



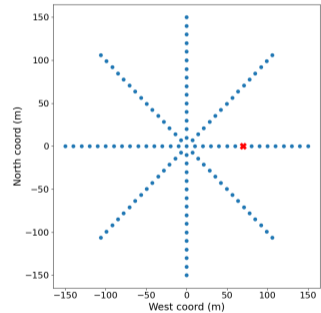
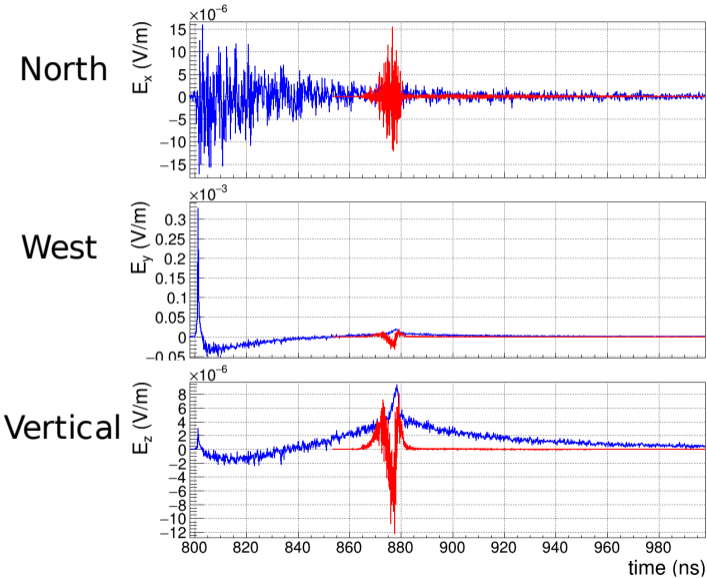
E for shower with $E_p = 10^{17}$ eV, $\theta = 0$, depth = -150 m



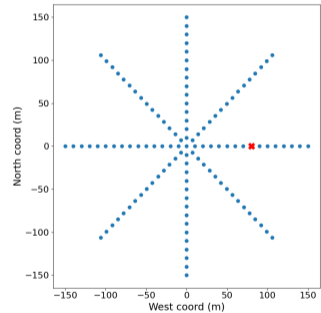
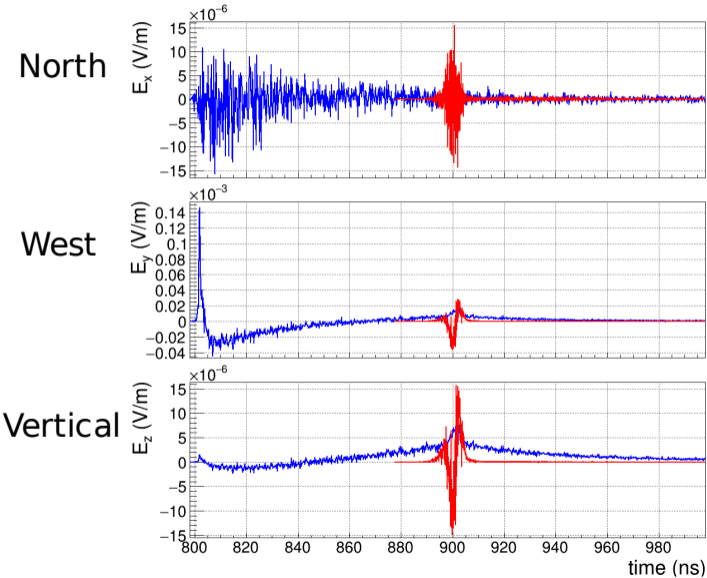
E for shower with $E_p = 10^{17}$ eV, $\theta = 0$, depth = -150 m



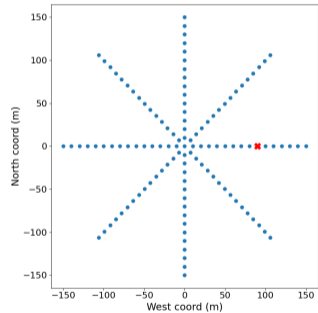
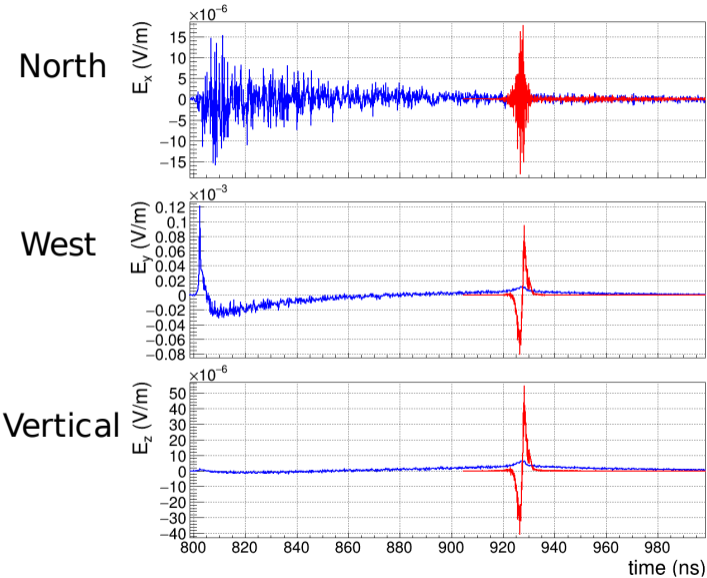
E for shower with $E_p = 10^{17}$ eV, $\theta = 0$, depth = -150 m



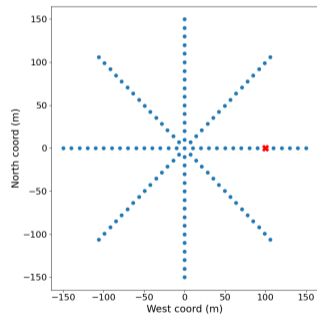
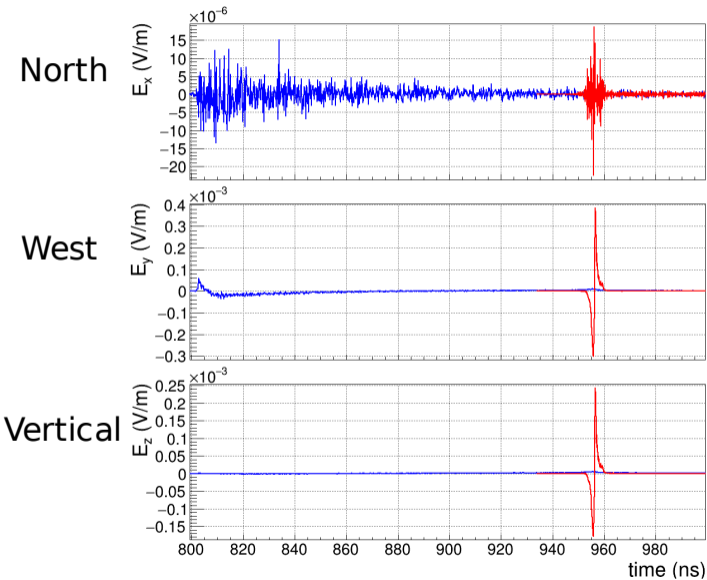
E for shower with $E_p = 10^{17}$ eV, $\theta = 0$, depth = -150 m



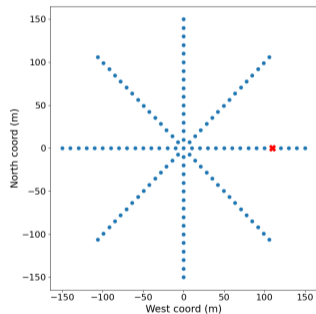
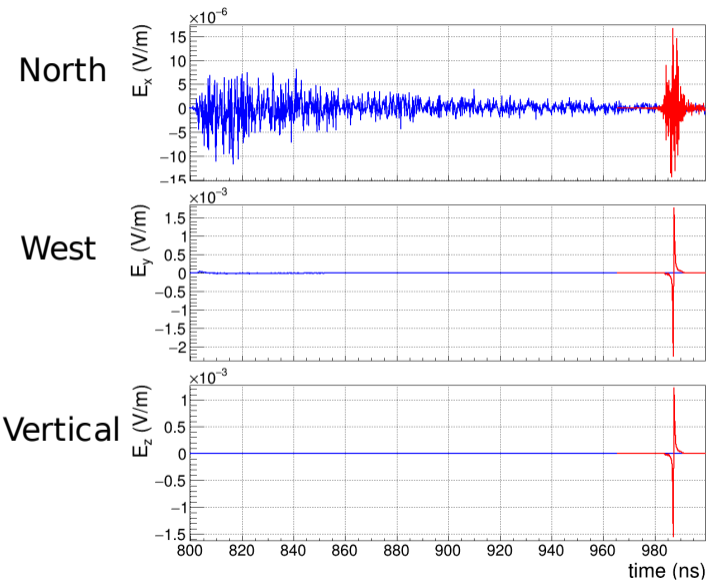
E for shower with $E_p = 10^{17}$ eV, $\theta = 0$, depth = -150 m



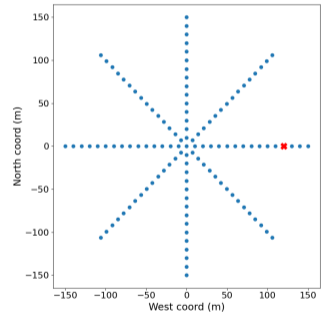
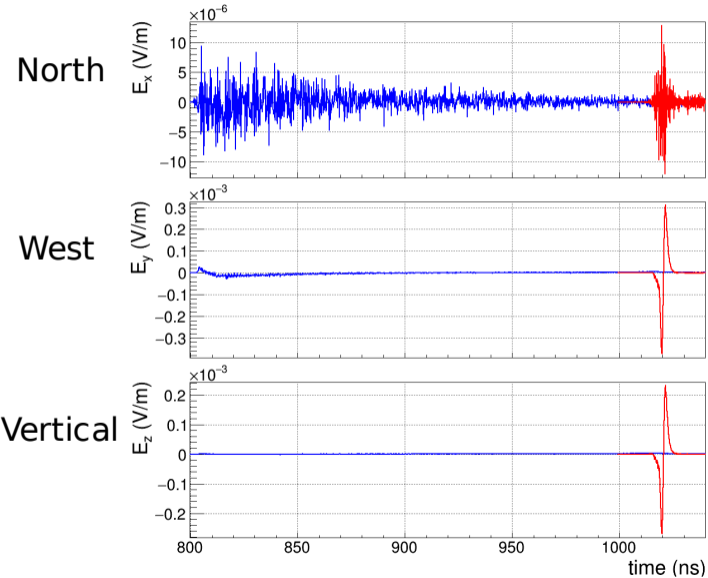
E for shower with $E_p = 10^{17}$ eV, $\theta = 0$, depth = -150 m



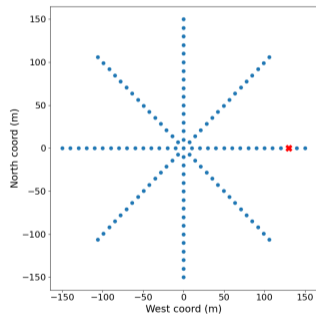
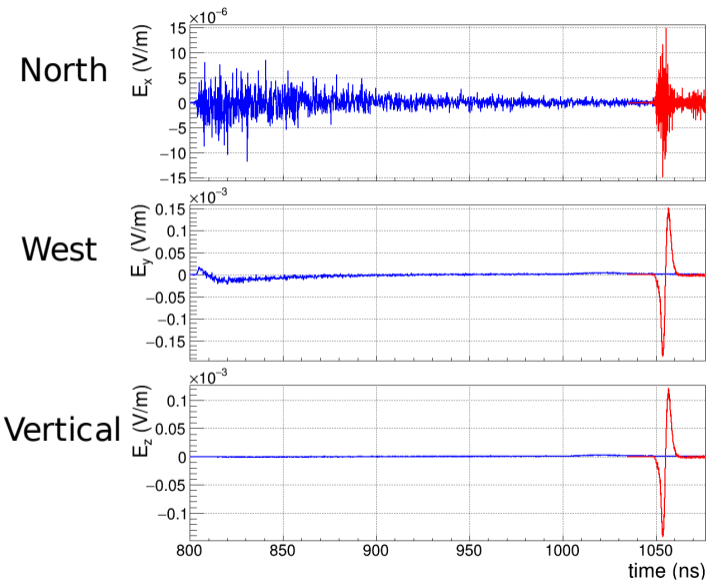
E for shower with $E_p = 10^{17}$ eV, $\theta = 0$, depth = -150 m



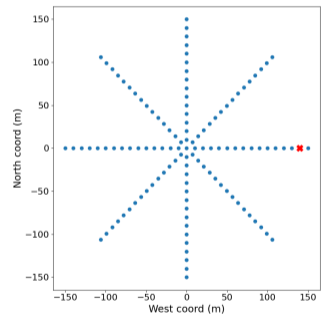
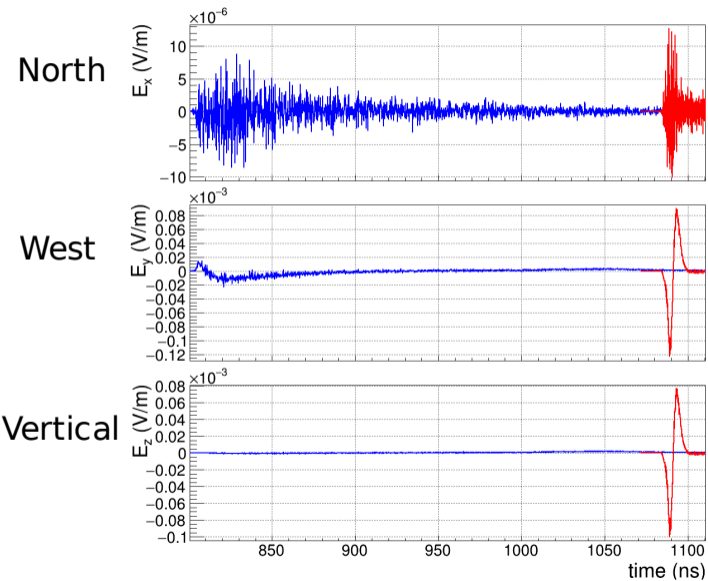
E for shower with $E_p = 10^{17}$ eV, $\theta = 0$, depth = -150 m



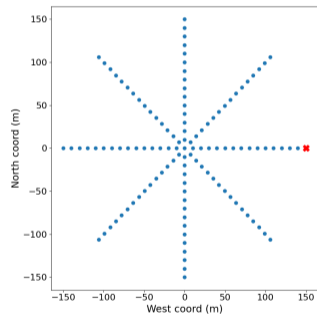
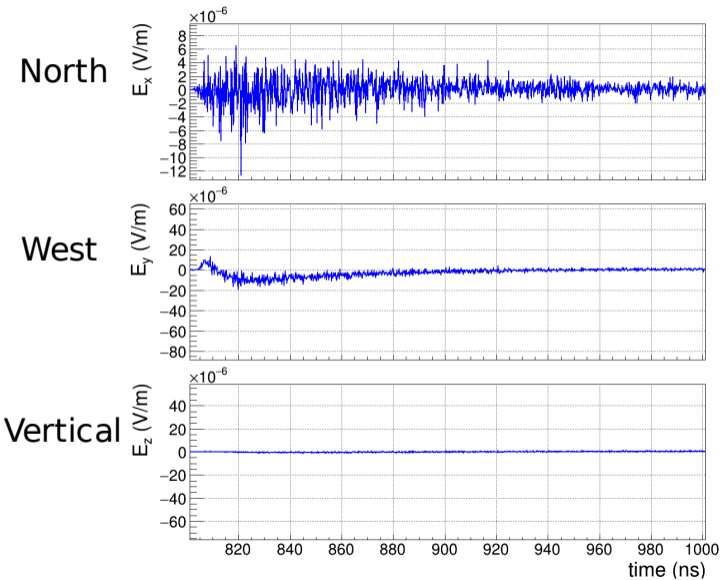
E for shower with $E_p = 10^{17}$ eV, $\theta = 0$, depth = -150 m



E for shower with $E_p = 10^{17}$ eV, $\theta = 0$, depth = -150 m



E for shower with $E_p = 10^{17}$ eV, $\theta = 0$, depth = -150 m



Conclusion

- The simulation is working well.
 - Analysing the results from first simulated showers.
- Simulating more shower geometries to get a better understanding.
- We can start exploring ways initiating comparisons with Corsika 8 and also porting the framework into Corsika 8.

Thank you!

“Adding” Raytracing to CoREAS

- CoREAS uses end point formalism to calculate E-field emissions.

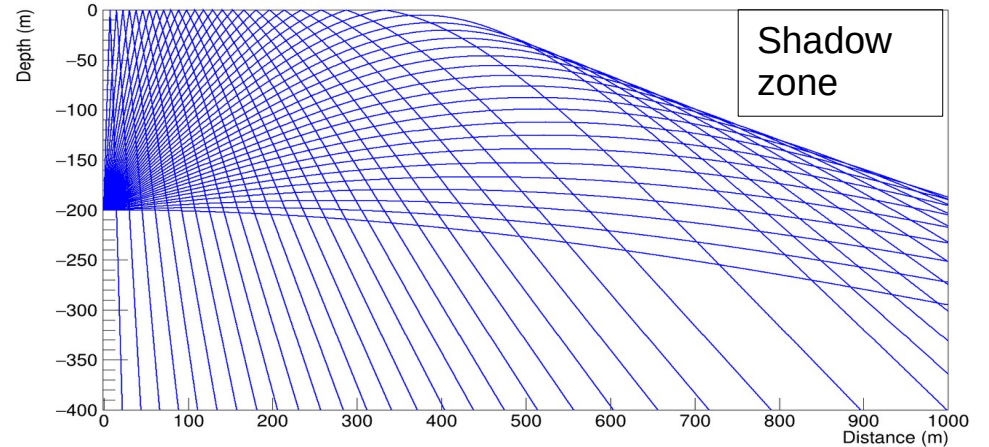
$$\vec{E}(\vec{x}, t) = \frac{q}{c} \left[\frac{\hat{r} \times [(\hat{r} - n\vec{\beta}) \times \dot{\vec{\beta}}]}{(1 - n\vec{\beta} \cdot \hat{r})^3 R} \right]_{ret}$$

- In this formula, I use the following raytracing parameters:
 - Launch angles as the dot product angle
 - Geometrical path length of the ray for the value R
 - The value of n is taken to be n at the emission point.

Raytracing in Polar Ice

- Rays are refracted owing to the depth-dependent density, and therefore index of refraction profile.
- For any given a transmitter and receiver geometry I have an analytic solution that traces out the rays in ice and air.
- The refractive index profile for SP ice:

$$n(z) = A + Be^{Cz} \quad , \text{ here } A=1.78, B=-0.43, C=-0.0132 \text{ 1/m}$$



Ray paths for a source at a depth of 200 m. The bending causes the formation of 'shadow zones'.

Air Refractive Index Profile

- Get the GDAS atmosphere file for a given set of GPS coordinates.
 - In this case its for a location close to South Pole.
- Get the five layer refractive index model using the GDAS file.

Layer	Altitude Range (m)	A	B	C (m^{-1})
1	0 to 3217.48	1	0.000328911	0.000123309
2	3217.48 to 8363.54	1	0.000348817	0.000141571
3	8363.54 to 23141.80	1	0.000361006	0.000145679
4	23141.80 to 100000	1	0.000368118	0.000146522
5	> 100000	1	0.000368117	0.000146522

A, B and C values for the five exponential refractive index layers of the South Pole atmosphere.

$$n(z) = A + Be^{Cz}$$

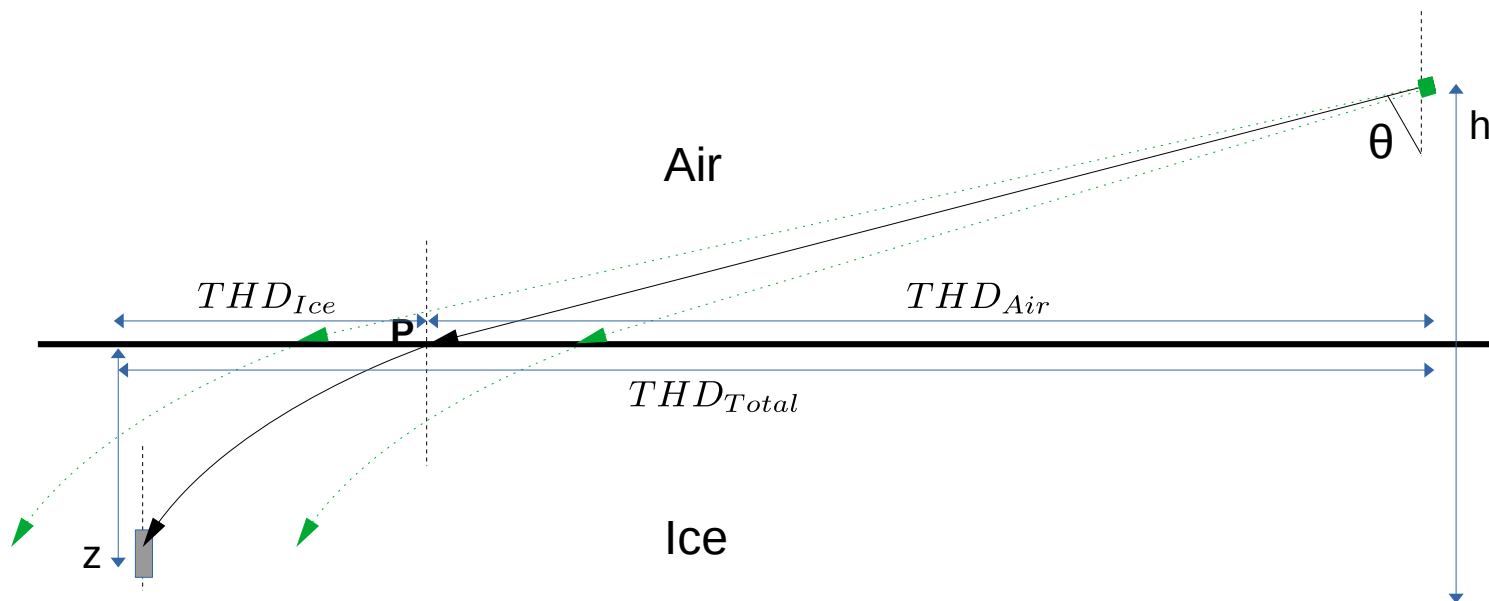
Launching Rays from Air to Ice

- Raytracing:
 - For a given transmitter receiver geometry we can always find the shortest possible path between them by minimizing the following expression:

$$f(\theta_s, h, z) = THD_{Air} + THD_{Ice} - THD_{Total} = 0,$$

Four parameters that define a Geometry

- 1) Transmitter altitude
- 2) Ice Layer Altitude
- 3) Antenna Depth
- 4) Total Horizontal Distance (THD)

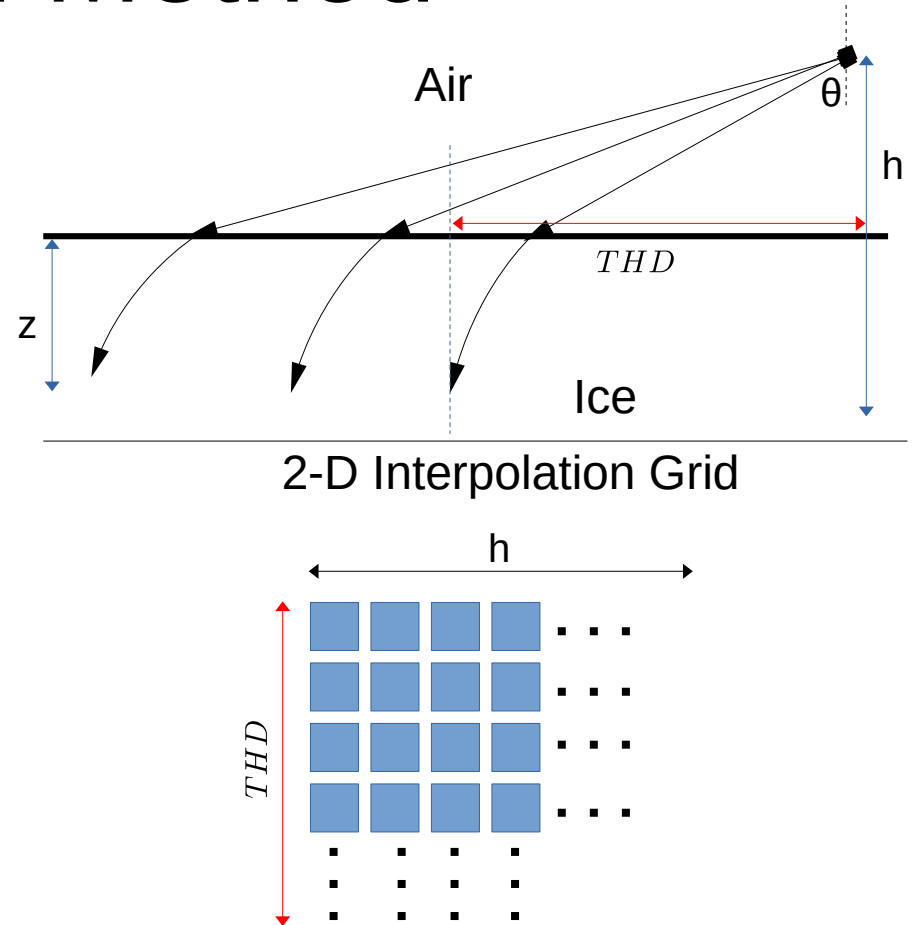


Raytracing Time

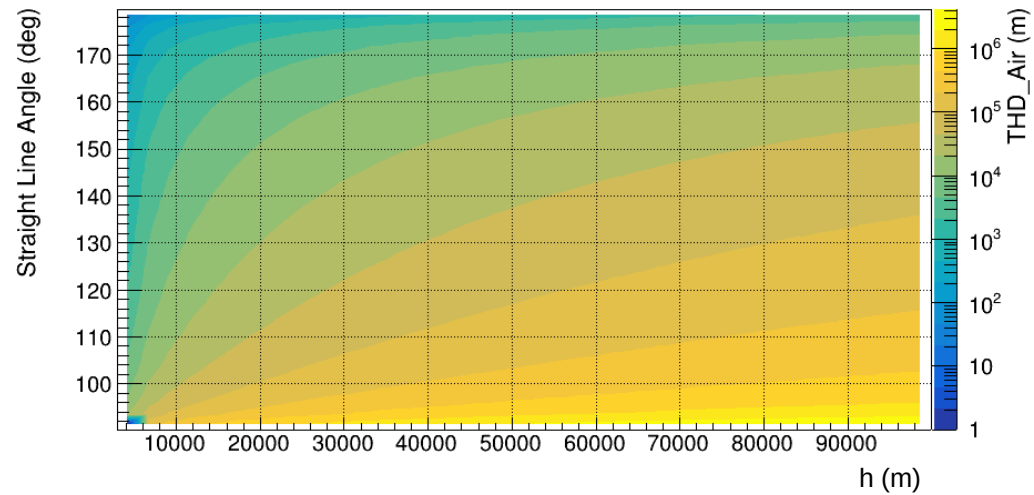
- So a typical raytracing call involving air and ice takes around 0.05 to 0.1 ms.
 - Currently making the atmosphere takes around 22 ms.
- Calling the analytic raytracing function for all shower particles ($\sim 10^9$) at all heights is still not feasible.
 - A shower will take around from a week to a month to simulate.
- Therefore, we have to move towards interpolation.

Interpolation Method

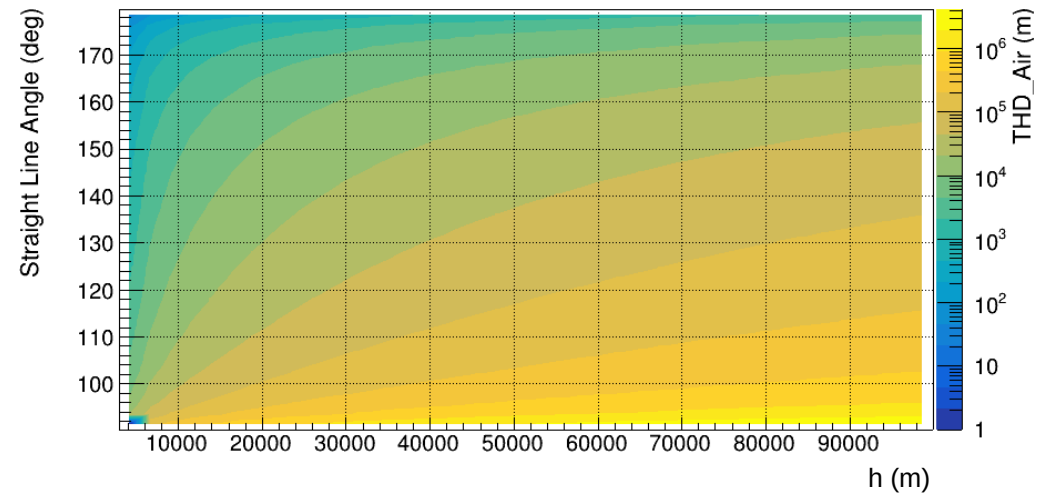
- For a given antenna depth I make 2-D grid of:
 - THD (Total Horizontal Distance)
 - The altitude of the in-air transmitter
- For each grid position I do analytic raytracing and store:
 - The initial launch angle of the ray
 - The total optical path length of the ray in air and in ice
 - The horizontal distance traveled by the ray in air and ice.
 - The angle of incidence on the ice surface and the Fresnel coefficients associated with it.
- Linear interpolation is used to calculate a given raytrace parameter.
 - It takes around 250 ns to do interpolation for each parameter.



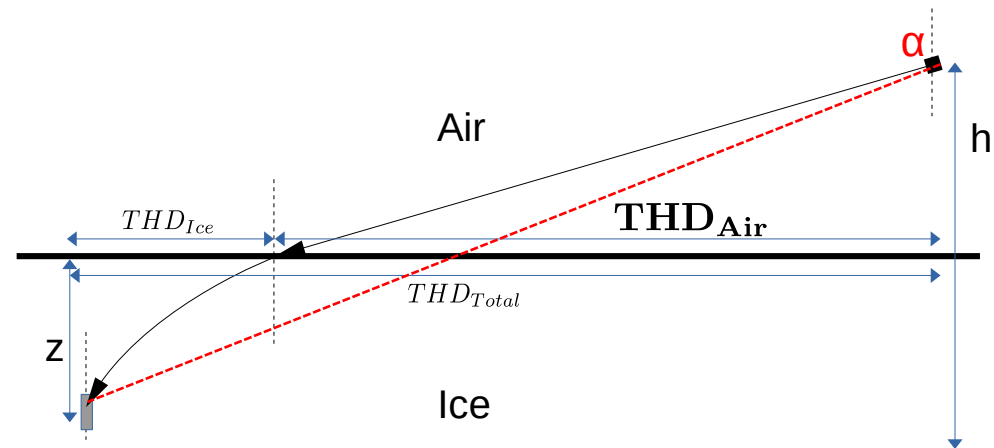
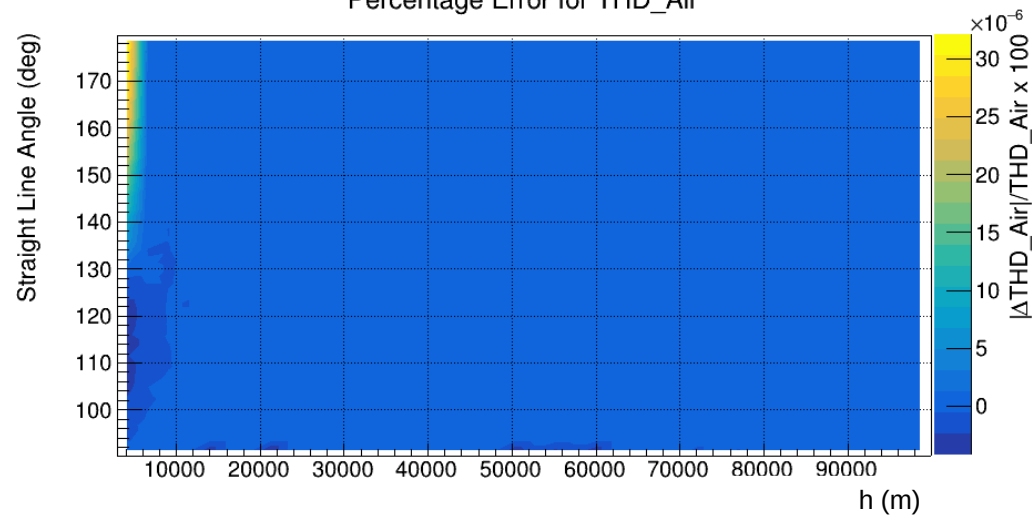
RayTrace results for THD_Air



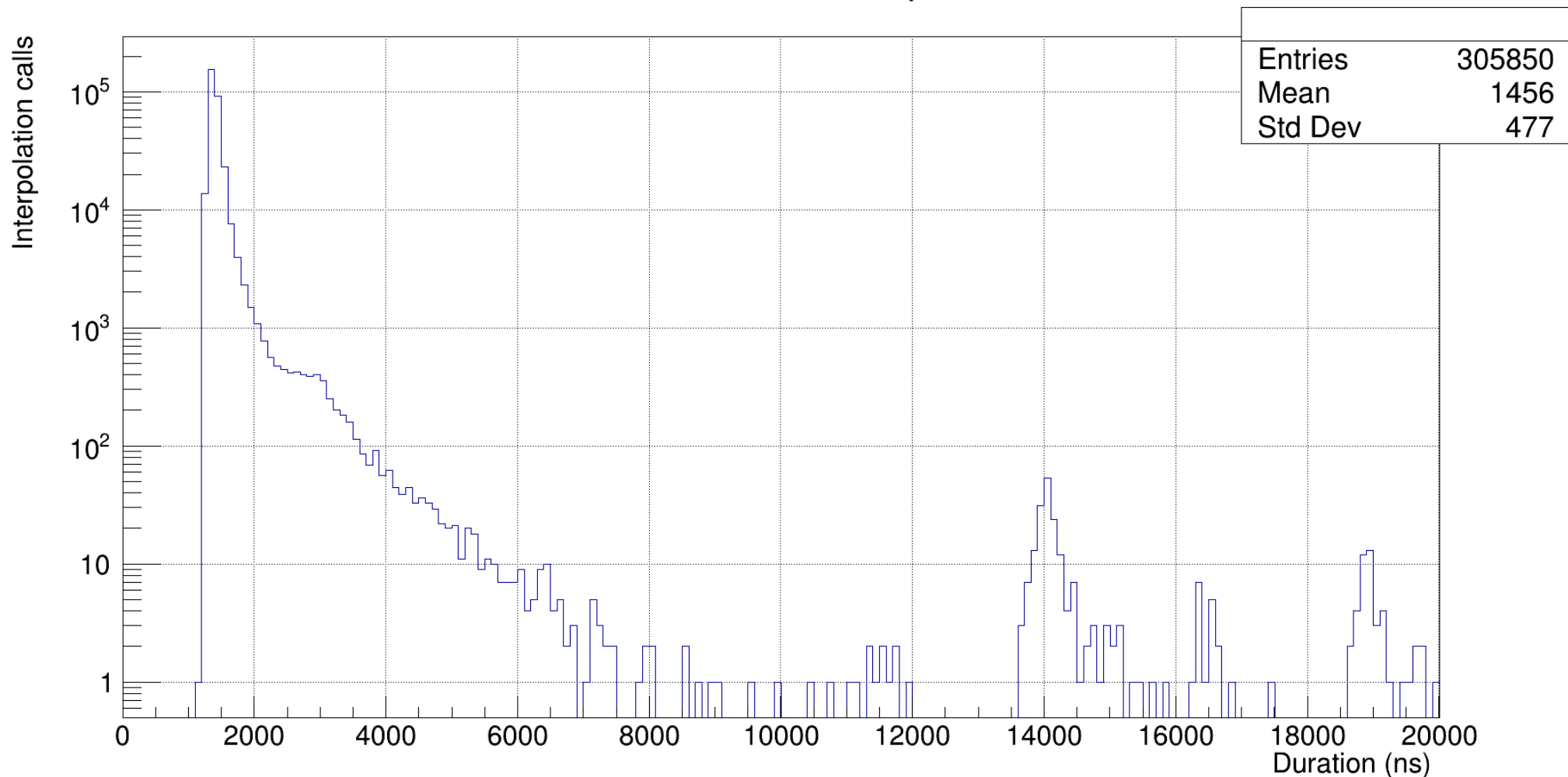
Interpolated results for THD_Air



Percentage Error for THD_Air



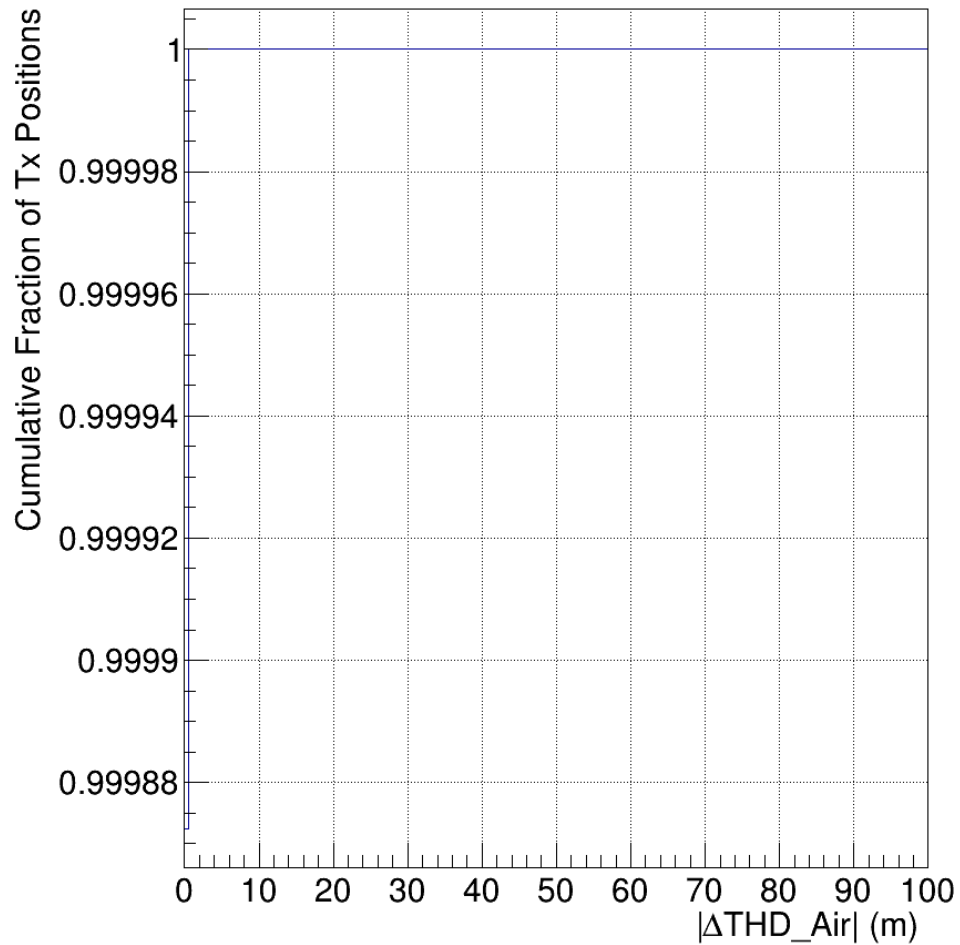
Time taken to do interpolation



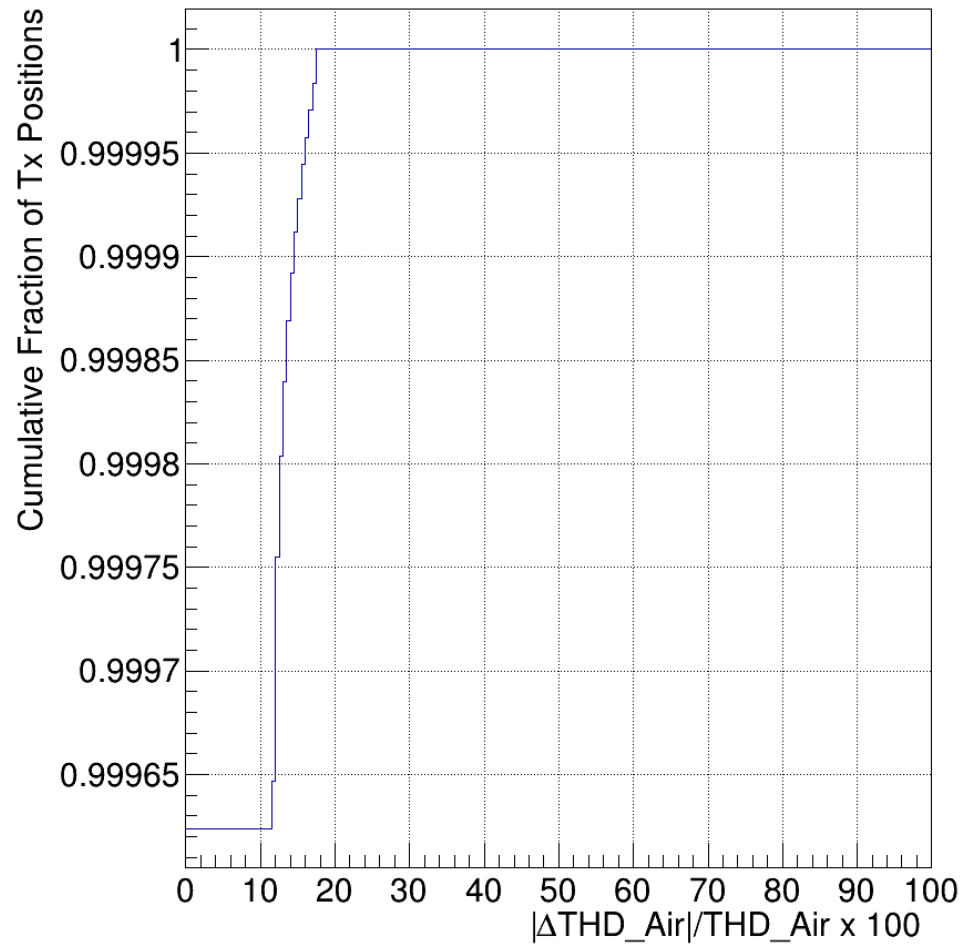
Interpolation Method

- θ (or the launch angle) has a step size of 0.1 deg and h has a step size of 10 m.
 - θ starts off at 90.1 deg and ends at 180.0 deg.
 - h starts off at 3000 m (the ice layer altitude) and ends at 100000 m.
- If the antenna depth changes we will need to make another 2-D grid for that.
- It takes around 60 ± 2 s to make the whole grid.
- For any given coordinate of (h, THD)
 - the closest h bins are calculated
 - The corresponding range of THDs for the h bins are found and the closest THD bins are found.
 - using the linear interpolation method the interpolation parameter value at the requested coordinate is calculated.

Absolute Error for THD_Air



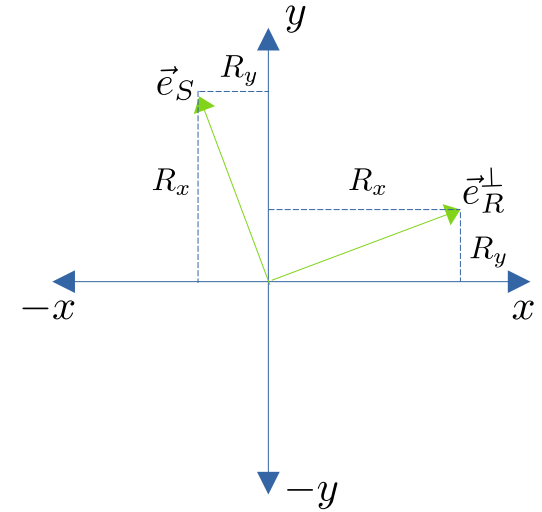
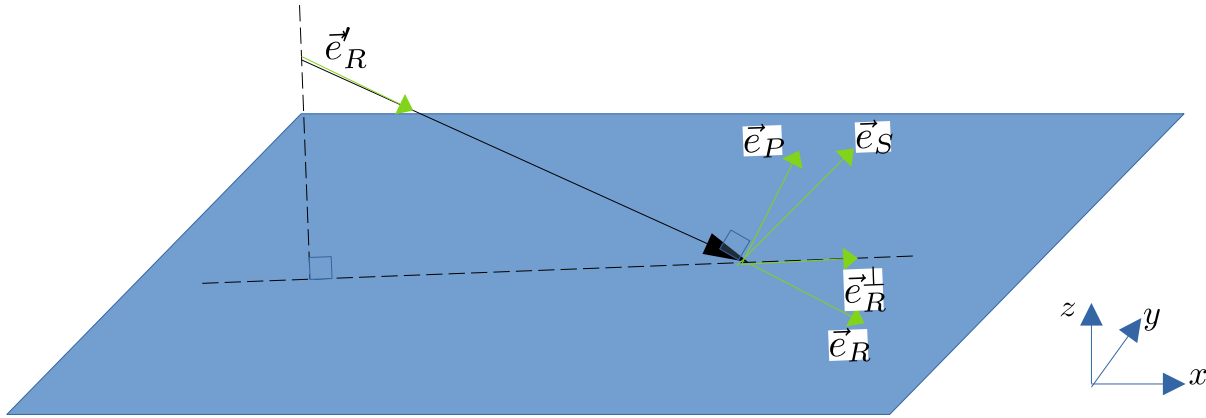
Percentage Error for THD_Air



Krijn's trick for calculating Fres. Coef

- We know that Fresnel coefficients should only depend on the angle of incidence of the ray.
- If we can parametrise the coefficients in terms of the angle of incidence (or the incidence vector) we can skip the whole rotation part.
 - Since we already know the angle of incidence from raytracing this should be straight forward.

Krijn's trick for Fresnel Coef. calculation



$$\vec{e}_R = (R_x, R_y, R_z) \quad (1)$$

$$\vec{e}_P = (P_x, P_y, P_z) \quad (2)$$

$$\vec{e}_S = (S_x, S_y, 0) \quad (3)$$

$$\vec{e}_R^\perp = (R_x, R_y, 0) \cdot \frac{1}{\sqrt{R_x^2 + R_y^2}} \quad (4)$$

\vec{e}_R = unit incidence vector

13/0 \vec{e}_R^\perp = unit launch vector

$\vec{e}_S \perp \vec{e}_R^\perp$ in the x-y plane

$$\vec{e}_S = (-R_y, R_x, 0) \cdot \frac{1}{\sqrt{R_x^2 + R_y^2}}$$

$$\vec{e}_P \perp \vec{e}_R \perp \vec{e}_S$$

$$\Rightarrow \vec{e}_P = \vec{e}_R \times \vec{e}_S = \begin{vmatrix} \hat{x} & -\hat{y} & \hat{z} \\ R_x & R_y & R_z \\ -R_y & R_x & 0 \end{vmatrix} \cdot \frac{1}{\sqrt{R_x^2 + R_y^2}}$$

$$\Rightarrow \vec{e}_P = \frac{1}{\sqrt{R_x^2 + R_y^2}} [-R_z R_x \hat{x} - R_z R_y \hat{y} + (R_x^2 + R_y^2) \hat{z}]$$

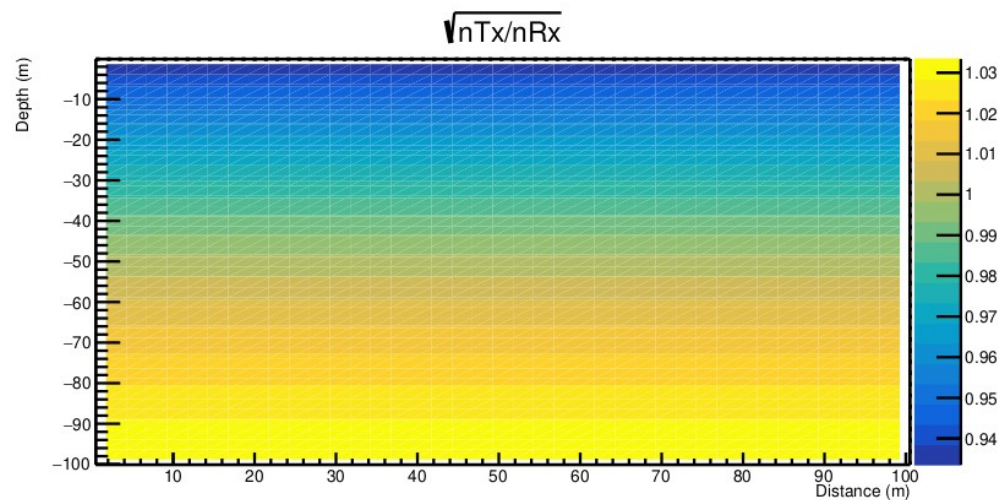
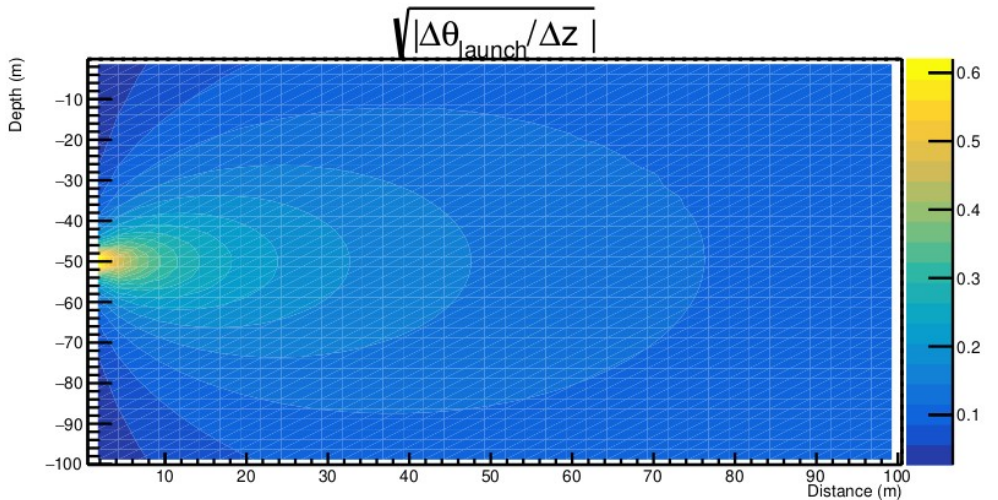
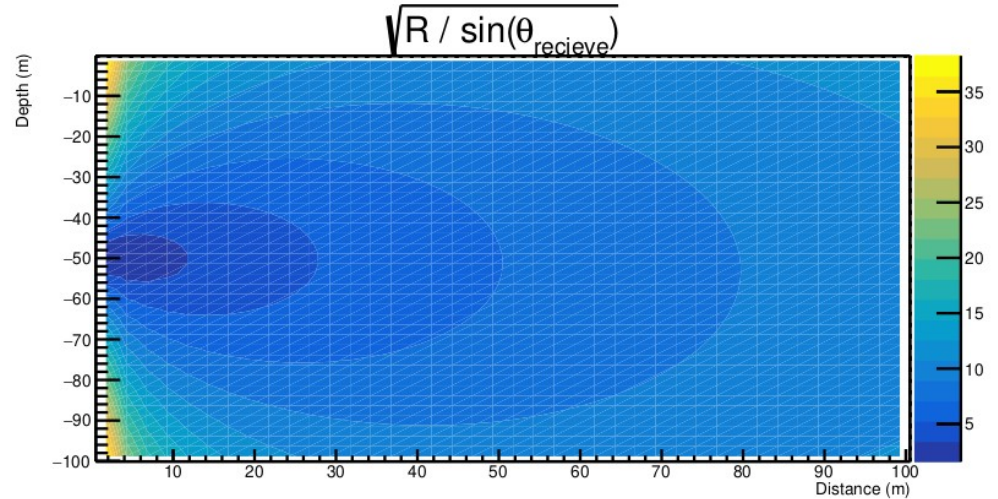
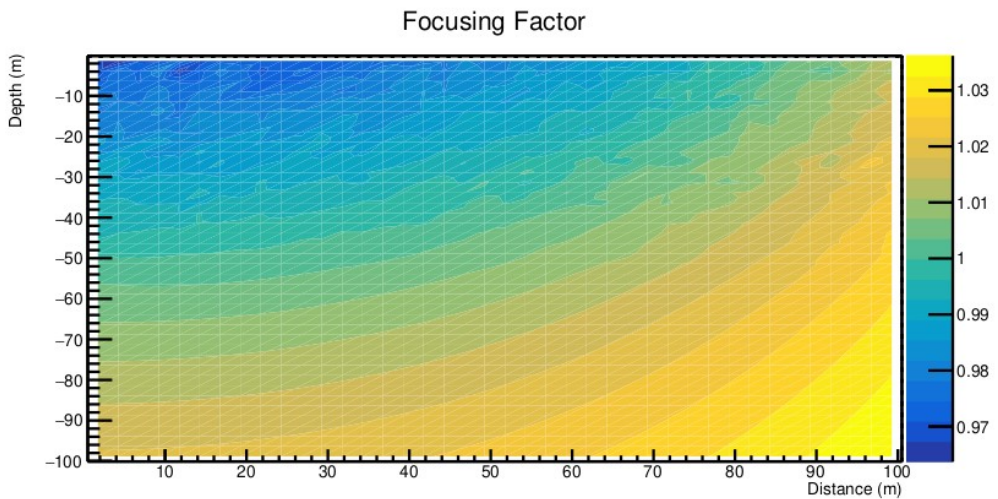
So effectively we have described the S and P vectors in terms of the vector of incidence.

So in order to apply Fresnel Coefficients to E-fields we will do:

$$E_s = \vec{E} \cdot \vec{e}_S \rightarrow E'_s \quad (1)$$

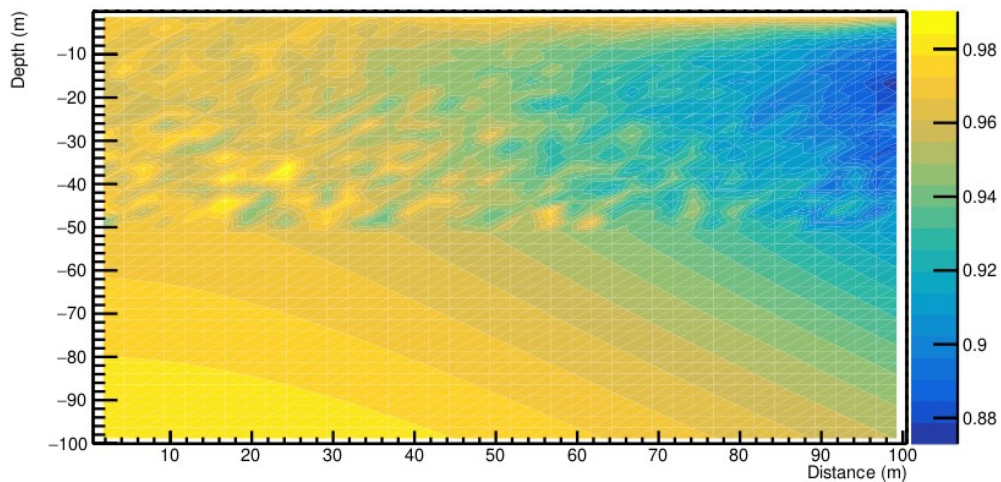
$$E_p = \vec{E} \cdot \vec{e}_P \rightarrow E'_p \quad (2)$$

Focusing Factor 1st ray 100 m

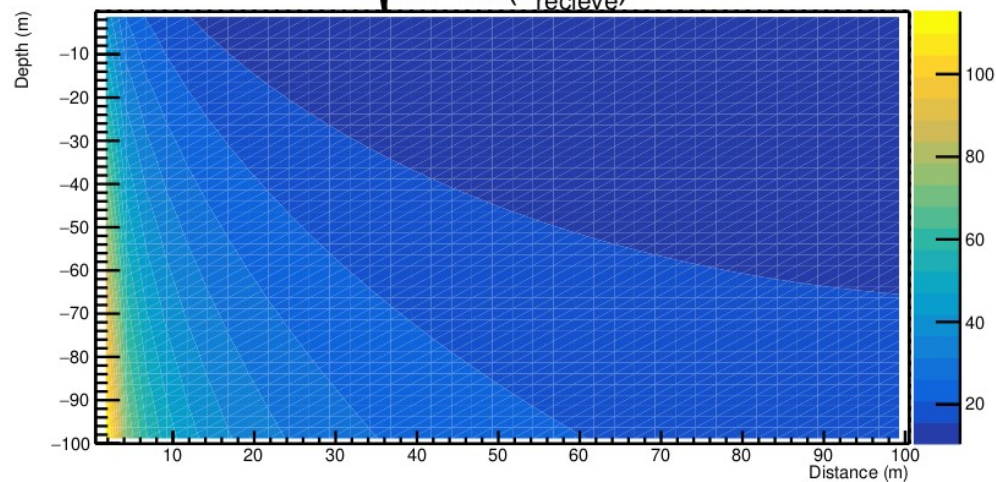


Focusing Factor 2nd ray 100 m

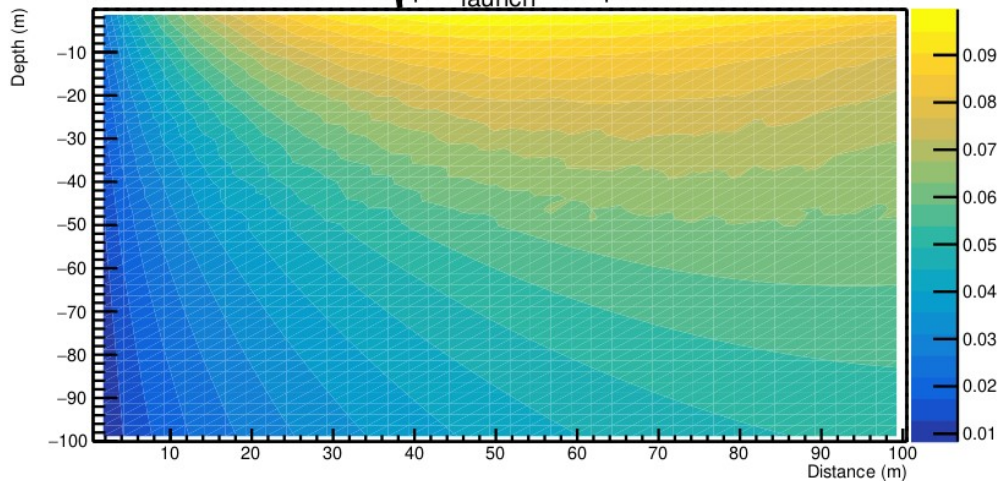
Focusing Factor



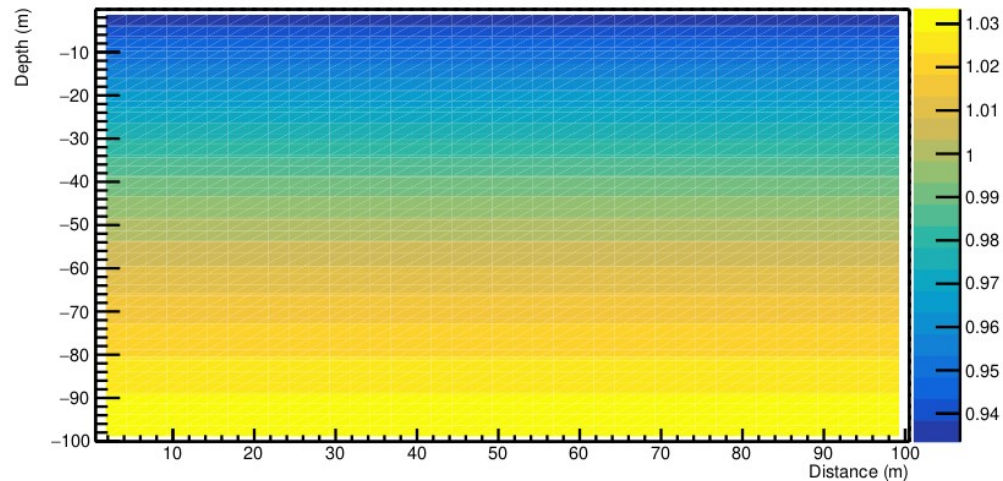
$\sqrt{R / \sin(\theta_{\text{recieve}})}$



$\sqrt{|\Delta\theta_{\text{launch}} / \Delta z|}$

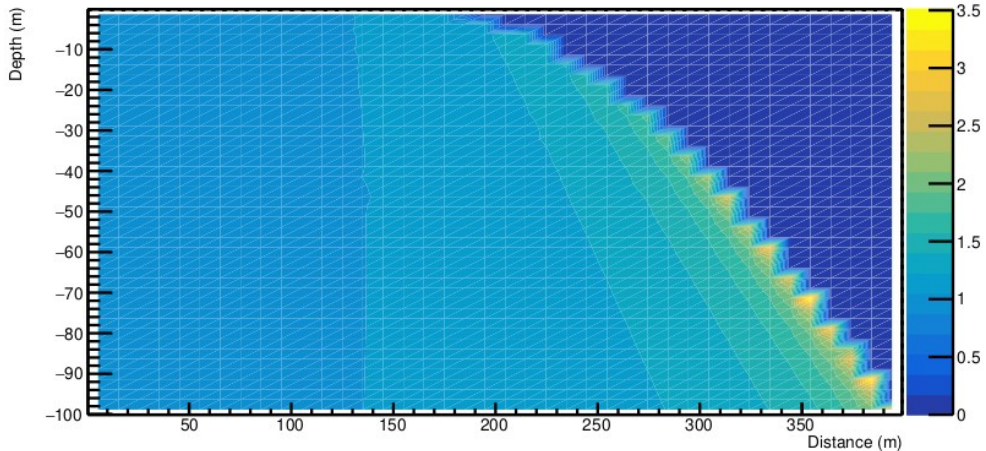


$\sqrt{n_{\text{Tx}} / n_{\text{Rx}}}$

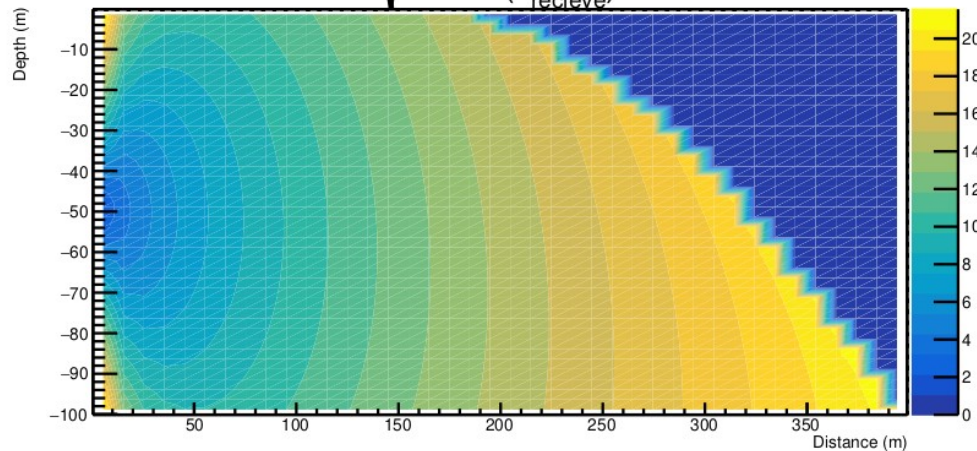


Focusing Factor 1st ray 400 m

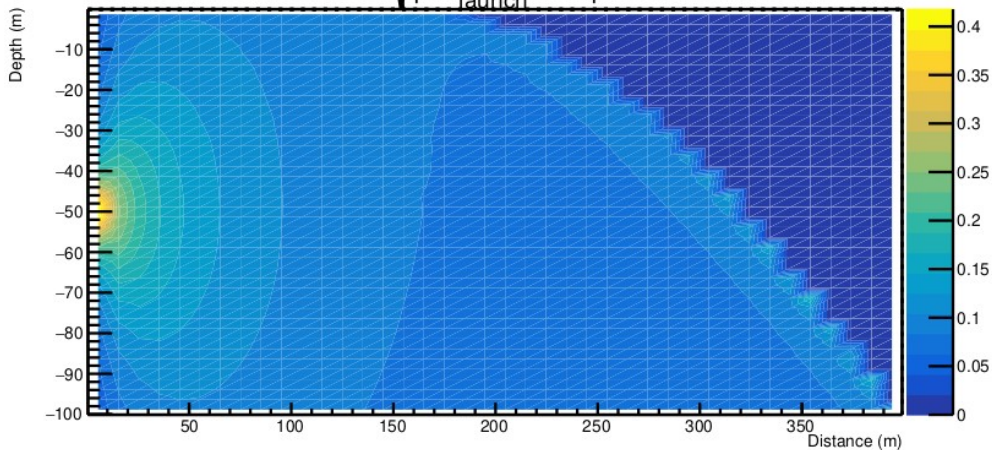
Focusing Factor



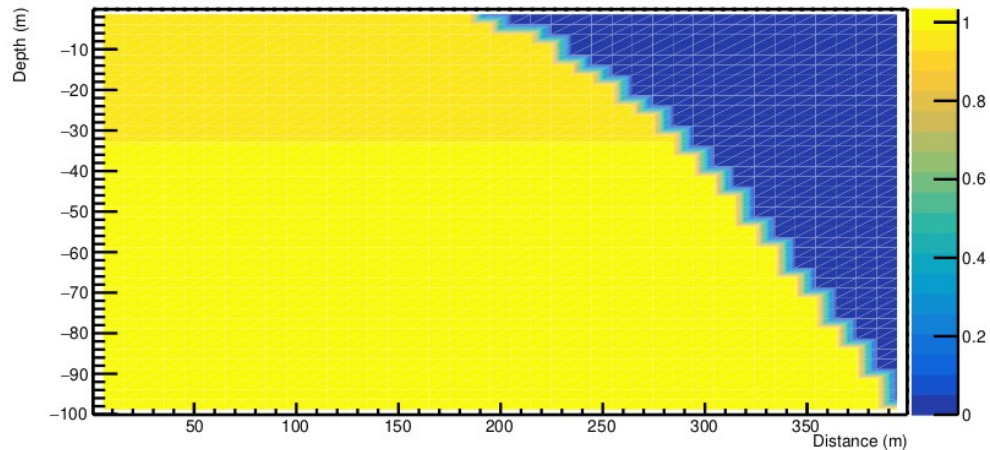
$\sqrt{R / \sin(\theta_{\text{recieve}})}$



$\sqrt{|\Delta\theta_{\text{launch}} / \Delta z|}$

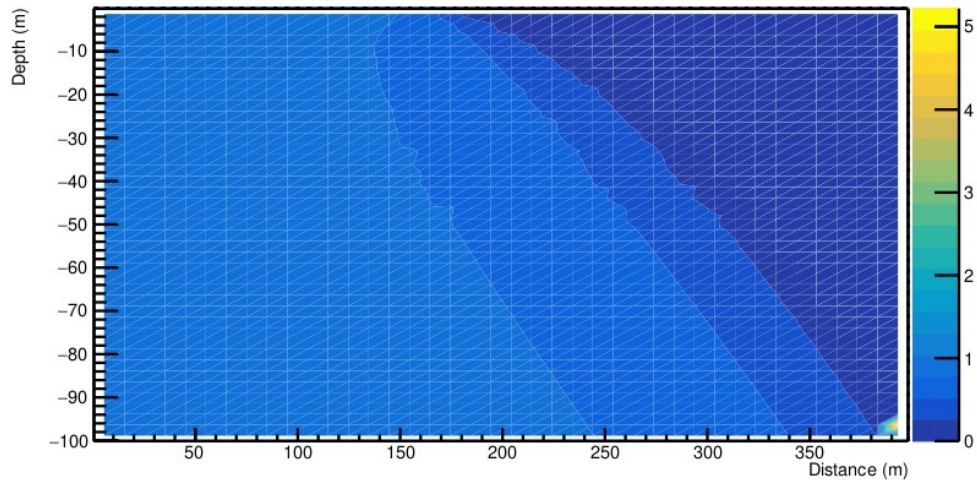


$\sqrt{n_{\text{Tx}}/n_{\text{Rx}}}$

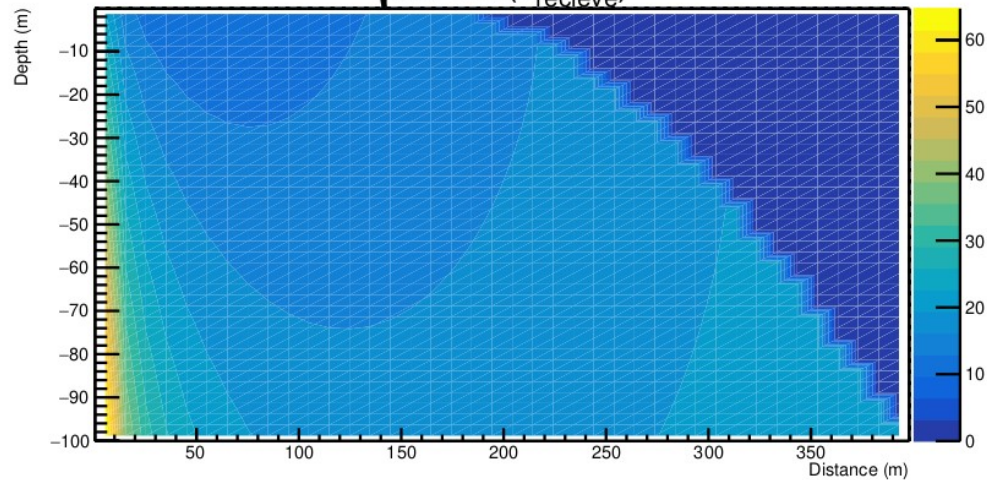


Focusing Factor 2nd ray 400 m

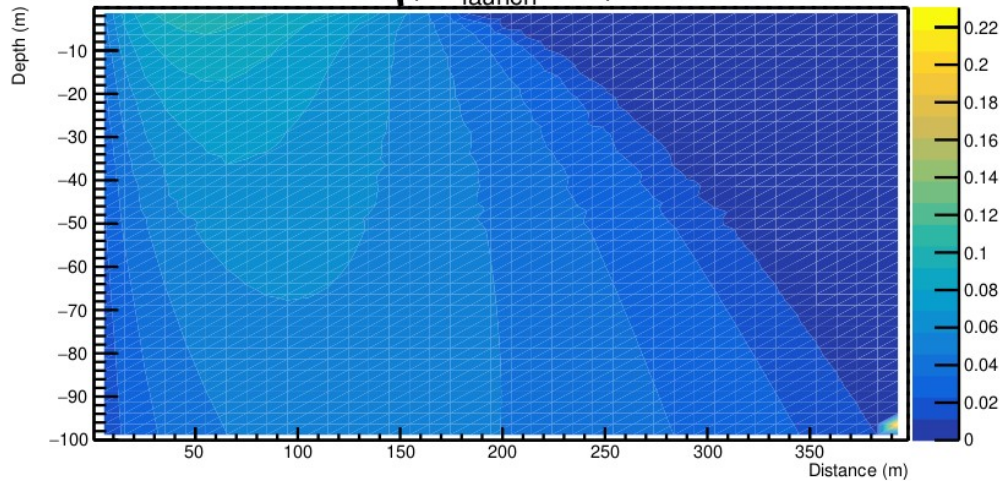
Focusing Factor



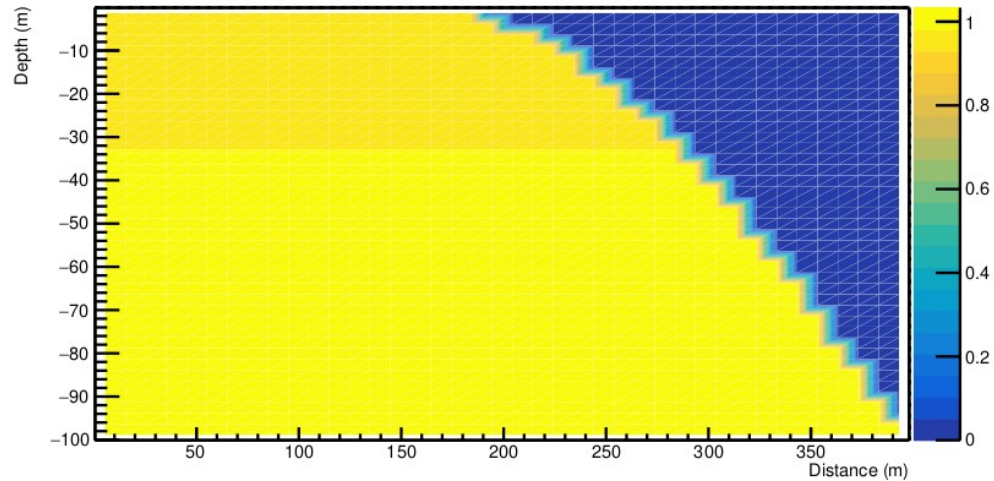
$\sqrt{R / \sin(\theta_{\text{recieve}})}$



$\sqrt{|\Delta\theta_{\text{launch}} / \Delta z|}$



$\sqrt{n_{\text{Tx}} / n_{\text{Rx}}}$



IN AIR BURSTS

WHY DOES THE BOOSTFACTOR MATTER?

The end point formalism (arxiv.org/abs/1112.2126) :

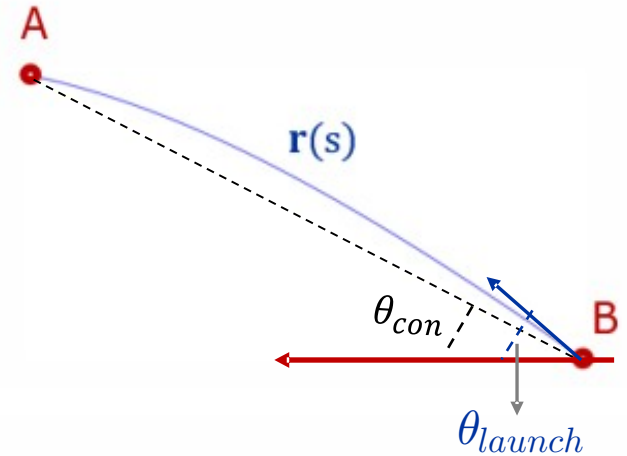
$$\vec{E}_{\pm}(\vec{x}, t) = \pm \frac{1}{\Delta t} \frac{q}{c} \left(\frac{\hat{r} \times [\hat{r} \times \vec{\beta}^*]}{\underbrace{(1 - n\vec{\beta}^* \cdot \hat{r})}_{\text{Boost factor}^{-1}}} R \right)$$

When calculating as $1 - n\beta \cos(\theta)$:

What n ?

What θ ?

Boost factor⁻¹



Previous studies (A. Timmermans, Ba. Thesis) show that a straight line approximation might not be valid for very inclined geometries in air

IN AIR BURSTS

WHAT ABOUT INCLINED SHOWERS?

The estimator with **local n and launch angle works** well here too!

The others do not agree

Similar results found by A.Timmermans

